

# Forwarding Design With Prescribed Local Behavior

M<sup>ed</sup> Sofiane Benachour, *Member, IEEE*, Vincent Andrieu, *Associate Member, IEEE*, Laurent Praly, *Member, IEEE*, and Hassan Hammouri

**Abstract**—Among the non-linear control techniques, some Lyapunov design methods (Forwarding/Backstepping) take advantage of the structure of the system (Feedforward-form/Feedback-form) to formulate a continuous control law which stabilizes globally and asymptotically the equilibrium. In addition to stabilization, we focus on the local behaviour of the closed loop system, providing conditions under which we can predetermine the behaviour around the origin for Feedforward systems.

**Index Terms**—Feedforward form, first order approximation, forwarding, Lyapunov design, stabilization.

## I. INTRODUCTION

THE synthesis of a stabilizing control law for systems described by nonlinear differential equations has been the subject of great interest by the nonlinear control community during the last three decades. Depending on the structure of the model, some techniques are now available to synthesize control laws ensuring global and asymptotic stabilization of the equilibrium point.

For instance, we can refer to the popular backstepping approach (see [1] and the reference therein or [2]), or the forwarding approach (see [3]–[6]) and some others based on energy considerations (see [7] for a survey of the available approaches).

Although the global asymptotic stability of the equilibrium point can be achieved in some specific cases, it remains difficult to address at the same time, performance issues of a nonlinear system in a closed loop. However, when the first order approximation of the non-linear model is considered, some performance aspects can be addressed by using linear optimal control techniques (using  $H_\infty$  controllers for instance).

Hence, it is interesting to raise the question of synthesizing a nonlinear control law which guarantees the global asymptotic stability of the origin while ensuring a prescribed local linear behavior. This type of question has been already discussed in the literature when backstepping design is used to synthesize a nonlinear continuous control law (see [8]).

In the present paper, we consider the same problem in the case of a system whose structure allows forwarding design techniques (see [4], [5]).

Manuscript received July 06, 2012; revised February 12, 2013; accepted June 21, 2013. Date of publication August 07, 2013; date of current version November 18, 2013. Recommended by Associate Editor L. Marconi.

M. S. Benachour, V. Andrieu, and H. Hammouri are with the Université de Lyon, Lyon F-69622, France and also with the Université Lyon 1, CNRS, UMR 5007, LAGEP (Laboratoire d'Automatique et de Génie des Procédés), Villeurbanne 69100, France (e-mail: benachour@lagep.univ-lyon1.fr; hammouri@lagep.univ-lyon1.fr).

L. Praly is with the Centre d'Automatique et Systèmes, Mines ParisTech, Fontainebleau 77305, France (e-mail: laurent.praly@ensmp.fr).

Color versions of one or more of the figures in this paper are available online at <http://ieeexplore.ieee.org>.

Digital Object Identifier 10.1109/TAC.2013.2277632

The paper is organized as follows. In Section II-A, the problem under consideration is described. Section II-B is devoted to the statement of the main theorem and to its discussion in the case of systems that are obtained after adding some dynamics composed of a neutrally stable part and integrations. Section IV gives an illustration of the results on a class of systems composed of a quadratic nonlinear part with a linear subsystem. Finally, Section V gives the conclusion.

## II. PROBLEM DESCRIPTION AND GENERAL RESULT

### A. Problem Description

To present the problem under consideration, we introduce a general controlled nonlinear system described by the following ordinary differential equation:

$$\dot{\chi} = \Phi(\chi, u) \quad (1)$$

with the state  $\chi$  in  $\mathbb{R}^N$  and  $\Phi : \mathbb{R}^N \times \mathbb{R}^m \rightarrow \mathbb{R}^N$  is a  $C^1$  function such that  $\Phi(0, 0) = 0$  and  $u$  is a control input in  $\mathbb{R}^m$ . For this system, we can introduce the two matrices describing its first order approximation at the origin which is assumed to be stabilizable

$$F := \frac{\partial \Phi}{\partial \chi}(0, 0), \quad G := \frac{\partial \Phi}{\partial u}(0, 0).$$

For system (1), the problem we intend to solve can be described as follows:

**Stabilization with prescribed local behavior:** Let the linear state feedback law  $u = K_o \chi$  stabilizing the first order approximation of system (1) be given. We are looking for a stabilizing control law  $\alpha_o : \mathbb{R}^N \rightarrow \mathbb{R}^m$ , differentiable at 0 such that:

- 1) the origin of the system

$$\dot{\chi} = \Phi(\chi, \alpha_o(\chi))$$

is globally and asymptotically stable.

- 2) The first order approximation of the control law  $\alpha_o$  satisfies

$$\frac{\partial \alpha_o}{\partial \chi}(0) = K_o.$$

A general answer to this problem has been given in [9], requiring the system to be input affine.

However, the set of local linear controllers  $K_o$  are those which satisfy a specific linear matrix inequality. Adding some structural constraints on the system (1) this problem has been addressed in [8] where the system is in strict feedback form.

In our study, we consider the case in which by decomposing the state as  $\chi = [y, x]$  the system (1) can be rewritten in the

following Feedforward form:

$$\begin{cases} \dot{y} = Ay + h(x), \\ \dot{x} = f(x) + g(x)u \end{cases} \quad (2)$$

with  $y$  in  $\mathbb{R}^{n_y}$ ,  $x$  in  $\mathbb{R}^{n_x}$  and with  $f : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^{n_x}$ ,  $g : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^{n_x \times m}$  and  $h : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^{n_y}$  are  $C^p$  functions,  $p \geq 2$  such that  $h(0) = 0$  and  $f(0) = 0$  and  $u$  is the control input in  $\mathbb{R}^m$ .

The stabilization problem for this class of system has been deeply studied in the last two decades employing forwarding techniques (see for instance [3]–[6], [10], [11]). Compared to our preliminary result in [12], the novelty comes from the fact that  $y$  is not a scalar.

The first order approximation of system (2) is denoted

$$\begin{cases} \dot{y} = Ay + Hx, \\ \dot{x} = Fx + Gu \end{cases} \quad (3)$$

with the matrices  $H$ ,  $F$  and  $G$  given as

$$F = \frac{\partial f}{\partial x}(0), \quad H = \frac{\partial h}{\partial x}(0), \quad G = g(0). \quad (4)$$

In the following, we make three structural Assumptions on the nonlinear system (2). The first one establishes that the first order approximation is stabilizable.

*Assumption 1:* The system (3) is stabilizable.

The second assumption we make is also a local property and concerns more specifically the vector field  $g(x) = (g_1(x), \dots, g_m(x))$ .

*Assumption 2:* The distribution  $\text{Vect}\{g_1(x), \dots, g_m(x)\}$  is involutive and of constant dimension  $m$  in a neighborhood of the origin.

In the case where there is only one input (i.e.,  $m = 1$ ), this assumption is always satisfied provided  $g(0) \neq 0$ .

In the spirit of [4], we make the following assumption on the matrix  $A$  in the  $y$  subsystem.

*Assumption 3:* There exists a positive definite matrix  $P$  in  $\mathbb{R}^{n_y \times n_y}$  such that the following equality holds:

$$PA + A'P = 0. \quad (5)$$

This Assumption implies that the matrix  $A$  has all its eigenvalues with zeros real part and we recover the case in which  $y$  is scalar as already studied in our preliminary conference paper [12].

Also, we assume that the stabilization problem with any prescribed local behavior can be solved for the  $x$  subsystem in system (2). More precisely, given  $p$  in  $\mathbb{N}$  we make the following assumption on the functions  $f$  and  $g$ :

*Assumption 4:* For all matrices  $K_x$  in  $\mathbb{R}^{m \times n_x}$  such that the matrix  $F + GK_x$  is Hurwitz, there exists a function  $\alpha_x : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^m$  of class  $C^p$  such that the following two properties are satisfied:

- 1) the origin of the system

$$\dot{x} = f(x) + g(x)\alpha_x(x) \quad (6)$$

is globally and asymptotically stable;

- 2) the first order approximation of this function satisfies

$$\frac{\partial \alpha_x}{\partial x}(0) = K_x. \quad (7)$$

## B. Main Result

We are now ready to state the main result which gives sufficient conditions guaranteeing that the stabilization with prescribed local behavior can be solved for system (2).

*Theorem 1 (Adding Integration With Prescribed Local Behavior):* Assume the System (2) satisfies Assumptions 1, 2, 3 and 4 for a given  $p$  in  $\mathbb{N}$ . Let a linear controller  $K_o = (K_{o,y}, K_{o,x})$  in  $(\mathbb{R}^{m \times n_y} \times \mathbb{R}^{m \times n_x})$  such that the matrix

$$\Psi = \begin{bmatrix} A & H \\ GK_{o,y} & F + GK_{o,x} \end{bmatrix} \quad (8)$$

is Hurwitz be given. Assume moreover that there exists a positive definite matrix  $\mathcal{P}$  defined as

$$\mathcal{P} = \begin{bmatrix} P & Q \\ Q' & R \end{bmatrix} \quad (9)$$

which satisfies the weak Lyapunov inequality

$$[\mathcal{P}\Psi + \Psi'\mathcal{P}] \leq -c_L \begin{bmatrix} QGG'Q' & 0 \\ 0 & S \end{bmatrix} \quad (10)$$

and where  $P$  is a positive definite matrix in  $\mathbb{R}^{n_y \times n_y}$  which satisfies (5) and where  $S$  is a  $n_x \times n_x$  positive definite matrix and  $c_L$  is a positive real number and  $QG$  is left invertible. Then there exists a  $C^{p-1}$  function  $\alpha_o : \mathbb{R}^{n_x+n_y} \rightarrow \mathbb{R}^m$  such that the following properties are satisfied:

- 1) the function  $\alpha_o$  satisfies

$$\frac{\partial \alpha_o}{\partial y}(0,0) = K_{o,y}, \quad \frac{\partial \alpha_o}{\partial x}(0,0) = K_{o,x}; \quad (11)$$

- 2) the origin of the system

$$\dot{y} = Ay + h(x), \quad \dot{x} = f(x) + g(x)\alpha_o(x, y), \quad (12)$$

is globally stable<sup>1</sup>. Moreover, if any forward bounded solution to the system

$$\dot{y} = Ay, \quad y'QG = 0 \quad (13)$$

defined on  $[0 + \infty[$ , converges to the origin then the origin is globally asymptotically stable.

## C. Discussion on Theorem 1

*1) About Assumption 4:* Assumption 4 is stronger than a stabilizability property since it is assumed that all local behaviors can be recovered for the closed loop system when considering the  $x$  dynamics only. However, employing the result obtained in [8], yields that Assumption 4 is satisfied in the case in which the  $x$  sub-system is in strict feedback form and when the functions

<sup>1</sup>An equilibrium point is said *globally stable* if it is stable and if all solutions are bounded (see [13, Page 40] for further details).

$f$  and  $g$  are sufficiently smooth. Note also that it is trivially satisfied when this system is a linear controllable system as studied in Section IV.

2) *About the Weak Linear Lyapunov Inequality:* The right hand side of inequality (10) may not be a full rank matrix. Indeed, this one is of rank  $n_x + m$ . In order to apply Theorem 1, we need to find  $\mathcal{P}$  solution to the weak Lyapunov inequality (10) and (5). Note that in the case there is one input (i.e.,  $m = 1$ ), this construction can be reformulated in terms of an equivalent linear matrix inequality. Indeed, we can show the following proposition.

**Proposition 1:** Let  $K_o = [K_{o,y}, K_{o,x}]$  in  $\mathbb{R}^n$  be given such that  $K_{o,y} \neq 0$ . Let  $P$  be a positive definite matrix in  $\mathbb{R}^{n_y \times n_y}$  which satisfies (5). The matrix  $\mathcal{P}$  defined in (9) satisfies (10) with  $QG \neq 0$  if and only if it satisfies the following linear matrix inequality:

$$\mathcal{P} > 0, [\mathcal{P}\Psi + \Psi'\mathcal{P}] \leq -c_L \begin{bmatrix} K'_{o,y}K_{o,y} & 0 \\ 0 & S \end{bmatrix}, S > 0. \quad (14)$$

*Proof:* Assume (14) is satisfied. Since  $K_{o,y} \neq 0$  this implies that  $QG \neq 0$ . Moreover with (5),  $\mathcal{P}\Psi + \Psi'\mathcal{P} \leq 0$  implies that  $QGK_{o,y} + K'_{o,y}G'Q'$  is a negative semidefinite matrix. For this property to hold, this implies that there exists a positive real number<sup>2</sup> $\lambda$  such that  $QG = -\lambda K'_{o,y}$ . Consequently (10) is satisfied. The proof that (10) implies (14) follows the same lines. ■

In the case in which  $n_y = 1$  (this implies that  $A = 0$ ) this assumption can always be satisfied (indeed, this is the usual Lyapunov inequality). However, this is not the case when  $n_y > 1$ . For instance, if we consider the case of a system whose first order approximation is a linear system of the form

$$\begin{cases} \dot{y}_1 = -y_2 \\ \dot{y}_2 = y_1 + x \\ \dot{x} = u \end{cases} \quad (15)$$

It is shown in Appendix A that for all stabilizing linear controllers in the form  $u = k_2 y_2 + k_x x$  where  $(k_2, k_x)$  are real numbers (i.e.,  $K_o = [K_{o,y}, K_{o,x}]$  with  $K_{o,y} = [0, k_2]$ ), it is not possible to find  $\mathcal{P}$  such that the weak Lyapunov inequality (10) is satisfied with  $QG \neq 0$ . Hence, our approach can't be applied for this stabilizing local control law.

3) *About the Result:* As mentioned in the previous comment, when  $n_y = 1$ , the weak linear Lyapunov inequality is satisfied for all stabilizing linear controller. Consequently when  $n_y = 1$ , the conclusion of Theorem 1 implies that Assumption 4 is valid for the entire system with stabilizer in  $C^{p-1}$ . Hence, with an iterative procedure, higher order systems can be considered. Indeed, let system (1) be with  $\chi = (y, z, x)$ , with  $z = (z_1, \dots, z_{n_z})$  in the form

$$\begin{cases} \dot{y} = Ay + h(x, z) \\ \dot{z}_1 = h_1(z_2, \dots, z_{n_z}, x), \\ \vdots \\ \dot{z}_{n_z} = h_{n_z}(x), \\ \dot{x} = f(x) + g(x)u \end{cases} \quad (16)$$

<sup>2</sup>Given two real vectors  $v_1$  and  $v_2$  of the same dimension such that the matrix  $v_1 v_2' + v_2 v_1'$  is negative semidefinite. Note that we have,  $(v_1 v_2' + v_2 v_1')(|v_2|v_1 + |v_1|v_2) = (|v_2|v_1 + |v_1|v_2)(v_1'v_2 + |v_1||v_2|)$ . Consequently,  $(v_1'v_2 + |v_1||v_2|)$  is an eigenvalue which is strictly positive unless  $v_1'v_2 = -|v_1||v_2|$ . Hence the result.

with  $x$  in  $\mathbb{R}^{n_x}$ ,  $z_i$  in  $\mathbb{R}$  and  $y$  in  $\mathbb{R}^{n_y}$ ,  $f : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^{n_x}$ ,  $g : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^m$  and  $h_i : \mathbb{R}^{n_z-i+n_x} \rightarrow \mathbb{R}$  are  $C^{i+2}$  functions, such that  $h_i(0, \dots, 0) = 0$  and  $f(0) = 0$  and  $u$  is the control input in  $\mathbb{R}$ . Based on the result obtained from Theorem 1, we can show the following result:

**Theorem 2 (Case of Higher Order Systems):** Assume the  $x$  subsystem of (16) satisfies Assumptions 2 and 4 with  $p = n_z + 2$ . Assume moreover the first order approximation of this system is stabilizable. For all vectors  $(K_{o,y}, K_{o,z}, K_{o,x})$  in  $(\mathbb{R}^{m \times n_y} \times \mathbb{R}^{m \times n_z} \times \mathbb{R}^{m \times n_x})$  which stabilizes globally and asymptotically the first order approximation of system (16) and such that there exists a matrix  $\mathcal{P}$  in the form (9) with  $Q$  in  $\mathbb{R}^{n_y \times (n_x + n_z)}$  which satisfies (10) with  $QG$  left invertible then there exists a  $C^1$  function  $\alpha_o : \mathbb{R}^{n_y + n_z + n_x} \rightarrow \mathbb{R}^m$  such that the following properties are satisfied :

1) the function  $\alpha_o$  satisfies

$$\begin{aligned} \frac{\partial \alpha_o}{\partial y}(0, 0, 0) &= K_{o,y}, \quad \frac{\partial \alpha_o}{\partial z}(0, 0, 0) = K_{o,z}, \\ \frac{\partial \alpha_o}{\partial x}(0, 0, 0) &= K_{o,x}; \end{aligned}$$

2) the origin of the system (16) in closed loop with  $u = \alpha_o(y, z, x)$  is globally stable and if moreover the origin is the only solution to the system (13) then the origin is globally asymptotically stable.

*Proof:* First, employing Theorem 1 it is shown that the  $(z_{n_z}, x)$ -subsystem in system (16) satisfies Assumption 4 with  $p = n_z + 1$ . Recursively, we apply again Theorem 1 and we obtain the result. ■

In the paper [9], the stabilization with prescribed local behavior has been addressed and studied on an inverted pendulum model. In some specific coordinates, this inverted pendulum model can be put in forwarding form and a forwarding control law has been introduced in [4]. It is noticed in [9] that, statistically, for all local behavior obtained from a  $LQ$  approach, the stabilization with prescribed local behavior could be solved. Consequently, Theorem 1 and Theorem 2 establish a theoretical justification on the fact that the approach of [9] applies on the forwarding model of the inverted pendulum.

#### PROOF OF THEOREM 1

The proof of this result is divided into four parts. In the first part, we focus on the linear approximation of the system and we show that the quadratic Lyapunov function associated with the local stabilizer (i.e.,  $\mathcal{P}$ ) can be rewritten in the form of a Lyapunov matrix that would have been obtained by following the forwarding design method of [4]. In the second part of the proof, we construct a candidate Lyapunov function  $V$  for the nonlinear model such that its quadratic approximation is the matrix  $\mathcal{P}$ . In the third part, from this candidate Lyapunov function we construct a control law which makes non positive the time derivative of the candidate Lyapunov function. By interpolating this control law with the local controller, we finally get our solution to the stabilization with prescribed local behavior. Finally, in the fourth part, we construct a Lyapunov function associated to this control law and show that LaSalle invariance principle may be applied to get asymptotic convergence of the closed loop trajectories toward the origin.

#### D. Part 1: Forwarding Local Lyapunov Function

In this part of the proof, we show that the weak Lyapunov matrix  $\mathcal{P}$  associated with the matrix  $\Psi$  can be rewritten in the form of a Lyapunov matrix that would have been obtained following the Forwarding design method of [4] or [6].

Indeed, note that the Lyapunov function associated to the matrix  $\mathcal{P}$  can be decomposed as follows:

$$\begin{bmatrix} y' & x' \end{bmatrix} \mathcal{P} \begin{bmatrix} y \\ x \end{bmatrix} = x' R_x x + (y - Mx)' P (y - Mx) \quad (17)$$

where  $R_x$  and  $M$  are, respectively, a matrix in  $\mathbb{R}^{n_x \times n_x}$  and a vector in  $\mathbb{R}^{n_x}$  defined as

$$R_x = R - Q' P^{-1} Q, \quad M = -P^{-1} Q. \quad (18)$$

If we compare the decomposition in (17) and the structure of the Lyapunov function obtained by the forwarding technique of [4] (see [6], (3)), we see that the matrix  $\mathcal{P}$  would be a Lyapunov matrix obtained by a forwarding design technique provided there exists  $K_x$  a vector in  $\mathbb{R}^{n_x}$  such that the following two requirements are satisfied:

- 1) There exists a matrix  $K_x$  in  $\mathbb{R}^{m \times n_x}$  which may differ from  $K_{o,x}$  and such that the following algebraic equation is satisfied (see [4, (132)]):

$$M(F + GK_x) = AM + H \quad (19)$$

- 2)  $u = K_x x$  is a control law for the  $x$ -subsystem associated to the Lyapunov matrix  $R_x$ . In other words,  $F + GK_x$  is a Hurwitz matrix and the following inequalities are satisfied:

$$R_x > 0, \quad R_x(F + GK_x) + (F + GK_x)' R_x < 0. \quad (20)$$

In this part of the proof we show that a vector  $K_x$  satisfying (19) and (20) does exist. Indeed, we can decompose  $\Psi = F + GK_o$  with<sup>3</sup>

$$F = \begin{bmatrix} A & H \\ 0_{n,1} & F \end{bmatrix}, \quad G = \begin{bmatrix} 0 \\ G \end{bmatrix}.$$

With these notation, we have

$$\mathcal{P}G = \begin{bmatrix} QG \\ RG \end{bmatrix}$$

and, employing the fact that  $PA + A'P = 0$  we get

$$\mathcal{P}F + F'\mathcal{P} = \begin{bmatrix} 0 & PH + QF + A'Q \\ Q'A + H'P + F'Q' & Q'H + RF + H'Q + F'R \end{bmatrix}.$$

Since we have assumed that  $QG$  is left invertible we can introduce the two matrices respectively in  $\mathbb{R}^{n_y \times n_x}$  and  $\mathbb{R}^{n_y \times n_y}$

$$\begin{aligned} w_1 &= -QG(G'Q'QG)^{-1}G'R, \\ w_2 &= QG(G'Q'QG)^{-1}G'Q' - I. \end{aligned} \quad (21)$$

<sup>3</sup>the symbol  $0_{a,b}$  stands for a  $a \times b$  zero matrix.

Note that we have

$$w_1'QG = -RG, \quad w_2'QG = 0.$$

Hence, we have for all  $n_x \times n_y$  real matrices  $\beta$

$$v'\mathcal{P}G = 0, \quad v = \begin{bmatrix} w_1 + w_2\beta \\ I_{n_x} \end{bmatrix}. \quad (22)$$

Note moreover that we have

$$v' \begin{bmatrix} QGG'Q' & 0 \\ 0 & S \end{bmatrix} v = S + RGG'R > 0.$$

Hence, it implies with (10)

$$v'[\mathcal{P}\Psi + \Psi'\mathcal{P}]v < 0.$$

This yields recalling that  $\Psi = F + GK_o$  and with (22)

$$v'[\mathcal{P}F + F'\mathcal{P}]v < 0. \quad (23)$$

More precisely, the following inequality is satisfied for all  $\beta$ :

$$\begin{aligned} v'[\mathcal{P}F + F'\mathcal{P}]v &= \beta'w_2'(PH + QF + A'Q) \\ &\quad + (H'P + F'Q' + QA)w_2\beta \\ &\quad + w_1'(PH + QF + A'Q) \\ &\quad + (H'P + F'Q' + QA)w_1 \\ &\quad + Q'H + RF + H'Q + F'R < 0. \end{aligned} \quad (24)$$

The matrix inequality (24) being true for all matrices  $\beta$ , it is for instance true for  $\beta = \alpha w_2'(PH + QF + A'Q)$  where  $\alpha$  is a positive real number. Hence we get

$$\begin{aligned} \alpha^2 [w_2'(PH + QF + A'Q)(H'P + F'Q' + QA)w_2] \\ + w_1'(PH + QF + A'Q) + (H'P + F'Q' + QA)w_1 \\ + Q'H + RF + H'Q + F'R < 0. \end{aligned}$$

Letting  $\alpha$  goes to infinity implies that we have

$$w_2'(PH + QF + A'Q) = 0. \quad (25)$$

This gives

$$QG(G'Q'QG)^{-1}G'Q'(PH + QF + A'Q) - PH - QF - A'Q = 0.$$

Consequently it yields

$$\begin{aligned} -Q[F + G[-(G'Q'QG)^{-1}G'Q'(PH + QF + A'Q)]] \\ = A'Q + PH. \end{aligned}$$

Left multiplying the previous equality by  $P^{-1}$  and employing the fact that with (5) we have  $P^{-1}A' = -AP^{-1}$  it yields

$$\begin{aligned} -P^{-1}Q \\ \times [F + G[-(G'Q'QG)^{-1}G'Q'(PH + QF + A'Q)]] \\ = A[-P^{-1}Q] + H. \end{aligned} \quad (26)$$

Hence, we recover (19) with  $M = -P^{-1}Q$  and

$$K_x = -(G'Q'QG)^{-1}G'Q'(PH + QF + A'Q). \quad (27)$$

It remains to check if  $K_x$  satisfies (20). Note that (24) and (25) imply that

$$w_1'(PH + QF + A'Q) + (H'P + F'Q' + QA)w_1 + Q'H + RF + H'Q + F'R < 0.$$

Replacing  $w_1$  by its definition given in (21) in the previous inequality yields

$$R(F + GK_x) + (F + GK_x)'R + Q'H + H'Q < 0. \quad (28)$$

On another hand, with (26), we have

$$Q'H = -Q'P^{-1}Q[F + GK_x] - Q'AP^{-1}Q.$$

Hence employing again  $P^{-1}A' = -AP^{-1}$ , inequality (28) becomes

$$S_x := R_x(F + GK_x) + (F + GK_x)'R_x < 0. \quad (29)$$

Therefore, for the time being, we showed this surprising property.

*Lemma 1:* Let  $\mathcal{P}$  be a matrix in the form (9) solution to the weak Lyapunov inequality (10) and such that its upper left block is a Lyapunov matrix associated to  $A$  (i.e., (5) is satisfied). Then this matrix can be decomposed in a forwarding-like manner. In other words,  $M$  and  $R_x$  defined in (18) satisfy (19) and (20).

From this crucial property, we will be able to get a candidate Lyapunov function for the nonlinear system associated to the local controller.

### E. Part 2: Construction of the Global CLF

In this part of the proof we construct a global (weak) control Lyapunov function denoted  $V_g$  for the nonlinear system (2) and such that its Hessian satisfies<sup>4</sup> $\mathcal{H}(V_g)(0) = 2\mathcal{P}$ . The construction of the candidate Lyapunov function is based on a modified forwarding technique inspired from [4] and employs Assumption 4. First, with Assumption 4, and the local stabilizer  $K_x$  given in (27), there exists a  $C^p$  function  $\alpha_x : \mathbb{R}^n \rightarrow \mathbb{R}^m$  such that the origin of the system (6) is globally and asymptotically stable and the local property (7) is satisfied.

Now, we can apply the following Lemma whose proof is given in Appendix B.

*Lemma 2:* There exists a  $C^\infty$  Lyapunov function  $V_x : \mathbb{R}^n \rightarrow \mathbb{R}_+$ , proper and positive definite, such that:

- $V_x$  is a Lyapunov function associated to the closed loop system (6). In other words, we have

$$-W_x(x) := \frac{\partial V_x}{\partial x}(x) [f(x) + g(x)\alpha_x(x)] < 0, \quad \forall x \neq 0. \quad (30)$$

- $V_x$  is locally quadratic and its local approximation is  $R_x$  defined in (18). We have

$$\mathcal{H}(V_x)(0) = 2R_x. \quad (31)$$

<sup>4</sup>The symbol  $\mathcal{H}$  denotes the operator which gives the Hessian of a given  $C^2$  function in  $\mathbb{R}^n$ .

For the non linear system (2), following the forwarding design described in [14] and [4], we can introduce the function  $\mathcal{M} : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^{n_y}$  defined as:

$$\mathcal{M}(x) = \int_{+\infty}^0 \exp(-As)h(X_1(x, s)) ds \quad (32)$$

where  $X_1(x, s)$  is the solution initiated from  $x$  and evaluated at time  $s$  of the system

$$\dot{x} = f(x) + g(x)\alpha_x(x).$$

The following Lemma can be obtained from [14, Lemma 6.88]. See also [5, Section 5.2] and [4].

*Lemma 3 ([14]):* The function  $\mathcal{M}$  defined in (32) is zero at the origin,  $C^p$  and satisfies the following partial differential equation:

$$\begin{aligned} \frac{\partial \mathcal{M}}{\partial x}(x) [f(x) + g(x)\alpha_x(x)] \\ = A\mathcal{M}(x) + h(x), \quad \forall x \in \mathbb{R}^n. \end{aligned} \quad (33)$$

With  $V_x$  obtained from Lemma 2, the function  $\mathcal{M}$  given in (32) we consider the  $C^p$  candidate Lyapunov function  $V_g : \mathbb{R}^{n+1} \rightarrow \mathbb{R}_+$  as

$$V_g(y, x) = V_x(x) + (y - \mathcal{M}(x))'P(y - \mathcal{M}(x)). \quad (34)$$

This function is proper and positive definite and, according to [4], it is a global weak CLF<sup>5</sup>.

To complete Part 2 of the proof, it remains to show the quadratic approximation of the candidate Lyapunov function is  $\mathcal{P}$ . More precisely, it remains to show that  $\mathcal{H}(V_g)(0, 0) = 2\mathcal{P}$ . Note that

$$\begin{aligned} \mathcal{H}(V_g)(0, 0) \\ = \begin{bmatrix} 2P & -2P \frac{\partial \mathcal{M}}{\partial x}(0) \\ -2 \left( \frac{\partial \mathcal{M}}{\partial x}(0) \right)' P & \mathcal{H}(V_x)(0) + 2 \left( \frac{\partial \mathcal{M}}{\partial x}(0) \right)' \frac{\partial \mathcal{M}}{\partial x}(0) \end{bmatrix}. \end{aligned} \quad (36)$$

By evaluating the partial derivative of (33) at the origin where  $f$ ,  $\alpha_x$  and  $h$  are zero, we get

$$\frac{\partial \mathcal{M}}{\partial x}(0)(F + GK_x) - A \frac{\partial \mathcal{M}}{\partial x}(0) = H.$$

The eigenvalues of  $(F + GK_x)$  and  $A$  being all different, the solution of this algebraic equation is unique and with (19), we get

$$\frac{\partial \mathcal{M}}{\partial x}(0) = M = -P^{-1}Q.$$

Hence, equality (36) becomes

$$\mathcal{H}(V_g)(0, 0) = 2 \begin{bmatrix} P & Q \\ Q' & R \end{bmatrix} = 2\mathcal{P}. \quad (37)$$

<sup>5</sup>Actually we can replace the function  $\mathcal{M}$  by its first order approximation at the origin namely we can replace  $\mathcal{M}(x)$  by  $\partial \mathcal{M} / \partial x(0)x = Mx$ . But then the Lyapunov function in (34) has to be modified in

$$V_g(y, x) = \ell(V_x(x)) + \left[ \sqrt{1 + (y - Mx)'P(y - Mx)} - 1 \right] \quad (35)$$

where  $\ell$  is a  $C^1$  class  $\mathcal{K}^\infty$  function to be tuned large (enough). For more details, see [4], [14] or [13].

### F. Part 3: Construction of the Controller

In this part of the proof we construct the global control law denoted  $\alpha_o$  solution to stabilization with prescribed local behavior problem. This one is obtained by interpolating  $K_o$  and a global control law  $\alpha_g$ .

By looking at the time derivative of  $V_g$  along the solution of the system (2), we see that a control law ensuring stabilization of the origin of the system (2) and boundedness of the solutions can be obtained simply<sup>6</sup> as

$$\alpha_g(y, x) = \alpha_x(x) - \frac{\partial V_x}{\partial x}(x)g(x) + 2(y - \mathcal{M}(x))'P \frac{\partial \mathcal{M}}{\partial x}(x)g(x).$$

Indeed, with (30) this gives along the trajectory of the system (2)

$$\begin{aligned} \left. \frac{d}{dt} V_g(y, x) \right|_{u=\alpha_g(y, x)} &= -W_x(x) \\ &- \left( \frac{\partial V_x}{\partial x}(x)Gg(x) - 2(y - \mathcal{M}(x))'P \frac{\partial \mathcal{M}}{\partial x}(x)g(x) \right)^2 \end{aligned} \quad (38)$$

which is non positive. But, unfortunately, the first order approximation of the control law  $\alpha_g$  is

$$K_g = \begin{bmatrix} \frac{\partial \alpha_g}{\partial y}(0, 0) & \frac{\partial \alpha_g}{\partial x}(0, 0) \end{bmatrix} = \begin{bmatrix} K_{g,x} & K_{g,y} \end{bmatrix}$$

with

$$K_{g,x} = K_x - 2G'R_x - 2G'M'PM, \quad K_{g,y} = 2G'M'P.$$

And this one is not equal to the given one  $K_o$ .

Hence the control law  $u = \alpha_g(y, x)$  is not a solution to the stabilization with prescribed local behavior.

The idea of the construction is to show that the two controllers  $u = \alpha_g(y, x)$  and  $u = K_{o,y}y + K_{o,x}x$  makes the time derivative of a same Lyapunov function non positive in a small neighborhood of the origin.

Indeed, we have the following lemma whose proof is given in appendix.

**Lemma 4 (Same Lyapunov Function for the two Controllers  $\alpha_g$  and  $K_o$ ):** There exist a positive definite function  $V_L : \mathbb{R}^{n_y} \times \mathbb{R}^{n_x} \rightarrow \mathbb{R}_+$  and three positive real numbers  $R_L$ ,  $c_g$  and  $c_o$  such that for all  $(y, x)$  such that  $V_L(y, x) \leq R_L$  we have

$$\left. \frac{d}{dt} V_L(y, x) \right|_{u=\alpha_g(y, x)} \leq -c_g (|x|^2 + |y'PMG|^2) \quad (39)$$

<sup>6</sup>Note that to design this control, we need to construct the function  $\mathcal{M}$  solution to the PDE (33). Hence, it may be difficult to apply this strategy for general feedforward systems. However, as shown in the following Section, when we consider some specific systems, this control law may be given in closed form. Moreover, when considering the Lyapunov function  $V_g$  given in (35) and provided we are able to compute the function  $\ell$ , an explicit solution may be given.

and

$$\left. \frac{d}{dt} V_L(y, x) \right|_{u=K_{o,y}y + K_{o,x}x} \leq -c_o [|x|^2 + |y'PMG|^2] \quad (40)$$

The proof of this Lemma relies on the use of change of coordinates which rectifies the controlled vector field  $g$  around the origin. This property relies on Assumption 2.

The two controllers  $K_o$  and  $\alpha_g$  making non positive the time derivative of the same Lyapunov function and the system being input affine it yields that any convex combination of both controllers will have the same property. Hence, we can interpolate in a neighborhood of the origin this control law with the prescribed one

$$\begin{aligned} \alpha_o(y, x) &= (1 - \rho(y, x))(K_{o,y}y + K_{o,x}x) + \rho(y, x)\alpha_g(y, x) \end{aligned} \quad (41)$$

with  $\rho$  any smooth function taking value in  $[0, 1]$  and such that

$$\rho(y, x) = \begin{cases} 0 & \text{if } V_L(y, x) \leq \frac{1}{3}R_L, \\ 1 & \text{if } V_L(y, x) \geq \frac{2}{3}R_L. \end{cases}$$

Indeed, in this case we get along the solution of the system (2) and for all  $(y, x)$  such that  $V_L(y, x) \leq R_L$

$$\begin{aligned} \left. \frac{d}{dt} V_L(y, x) \right|_{u=\alpha_o(y, x)} &= (1 - \rho(y, x)) \left. \frac{d}{dt} V_L(y, x) \right|_{u=K_{o,y}y + K_{o,x}x} \\ &+ \rho(y, x) \left. \frac{d}{dt} V_L(y, x) \right|_{u=\alpha_g(y, x)} \leq 0. \end{aligned}$$

This is sufficient to conclude that we have stability of the equilibrium. Note however that in order to study its asymptotic behavior and its convergence toward zero we make in the following section an analysis by introducing a Lyapunov function associated to our controller.

### G. Part 4: Modification of the Global CLF to Prove Asymptotic Stability

In this part, we unite the two functions  $V_g$  and  $V_L$  in order to obtain a Lyapunov function associated to the controller  $\alpha_o$ . Following [15] consider the function  $V_o$  defined as

$$\begin{aligned} V_o(y, x) &= \gamma(V_L(y, x))V_L(y, x) \\ &+ d[1 - \gamma(V_L(y, x))]V_g(y, x) \end{aligned}$$

where  $\gamma$  is any smooth and non increasing function such that

$$\gamma(s) = \begin{cases} 0 & \text{if } s \geq R_L, \\ 1 & \text{if } s \leq \frac{2}{3}R_L \end{cases}$$

and  $d$  is a positive real number such that

$$V_L(y, x) \leq dV_g(y, x), \quad \forall (y, x) : \frac{2}{3}R_L \leq V_L(y, x) \leq R_L.$$

Note that we have with  $u = \alpha_o(y, x)$

$$\begin{aligned} & \left. \dot{V}_o(y, x) \right|_{u=\alpha_o(y, x)} \\ &= \gamma'(V_L(y, x)) [V_L(y, x) - dV_g(y, x)] \left. \dot{V}_L(y, x) \right|_{u=\alpha_o(y, x)} \\ &+ \gamma(V_L(y, x)) \left. \dot{V}_L(y, x) \right|_{u=\alpha_o(y, x)} \\ &+ d(1 - \gamma(V_L(y, x))) \left. \dot{V}_g(y, x) \right|_{u=\alpha_o(y, x)} \end{aligned}$$

and different cases may be distinguished:

- 1) If  $V_L(y, x) \geq R_L$ . In this case, we have  $\alpha_o(y, x) = \alpha_g(y, x)$ ,  $\gamma'(V_L(y, x)) = 0$  and  $\gamma(V_L(y, x)) = 0$ . Consequently, we get

$$\begin{aligned} & \left. \dot{V}_o(y, x) \right|_{u=\alpha_o(y, x)} = -dW_x(x) \\ & - d \left( \frac{\partial V_x}{\partial x}(x) Gg(x) - 2(y - \mathcal{M}(x))' P \frac{\partial \mathcal{M}}{\partial x}(x) Gg(x) \right)^2. \end{aligned}$$

- 2) If  $R_L \geq V_L(y, x) \geq 2/3R_L$ . In this case, we have  $\alpha_o(y, x) = \alpha_g(y, x)$ . Consequently, we have  $\left. \dot{V}_L(y, x) \right|_{u=\alpha_o(y, x)} \leq 0$  and  $\left. \dot{V}_g(y, x) \right|_{u=\alpha_o(y, x)} \leq 0$ . Moreover we have  $V_L(y, x) - dV_g(y, x) \leq 0$  and  $\gamma'(V_L(y, x)) \leq 0$ . Hence, with (39) it yields

$$\begin{aligned} & \left. \dot{V}_o(y, x) \right|_{u=\alpha_o(y, x)} \leq \\ & - c_g \gamma(V_L(y, x)) [|x|^2 + |y' PMG|^2] \\ & - d(1 - \gamma(V_L(y, x))) [W_x(x) \\ & + \left( \frac{\partial V_x}{\partial x}(x) Gg(x) - 2(y - \mathcal{M}(x))' P \frac{\partial \mathcal{M}}{\partial x}(x) Gg(x) \right)^2]. \end{aligned}$$

- 3) If  $2/3R_L \geq V_L(y, x)$ . We have  $\gamma'(V_L(y, x)) = 0$  and  $\gamma(V_L(y, x)) = 1$ . Hence, it yields

$$\left. \dot{V}_o(y, x) \right|_{u=\alpha_o(y, x)} = \gamma(V_L(y, x)) \left. \dot{V}_L(y, x) \right|_{u=\alpha_o(y, x)}.$$

On another hand we have

$$\begin{aligned} & \left. \dot{V}_L(y, x) \right|_{u=\alpha_o(y, x)} \\ &= (1 - \rho(y, x)) \left. \dot{V}_L(y, x) \right|_{u=(K_{o,y}y + K_{o,x}x)} \\ &+ \rho(y, x) \left. \dot{V}_L(y, x) \right|_{u=\alpha_g(y, x)}. \end{aligned}$$

Hence

$$\begin{aligned} & \left. \dot{V}_L(y, x) \right|_{u=\alpha_o(y, x)} \leq \\ & - [c_o(1 - \rho(y, x)) + c_g \rho(y, x)] [|x|^2 + |y' MG|^2]. \end{aligned}$$

Hence, we get global stability and local asymptotic stabilization. Moreover, the control law satisfies the local property requested.

Finally, from LaSalle invariance principle, it follows that, for each trajectory, there exists a real number  $v$  such that it converges the trajectories converge to the largest set of points  $(y, 0)$ , invariant for the system

$$\dot{y} = Ay$$

and satisfying

$$V_o(y, 0) = v, \quad y' PMG = 0.$$

Recalling that  $M = -P^{-1}Q$ , we get the result.

### III. ILLUSTRATION ON A PARTICULAR CLASS OF SYSTEMS

In this section, we consider the problem of designing a robust stabilizing control law for a class of disturbed strict feedforward systems with linear  $x$  dynamics and a quadratic function  $h$ . In other words we consider the case in which the system (2) is in the form

$$\begin{cases} \dot{y} = Ay + h(x) + d_y(y, x)\omega \\ \dot{x} = Fx + Gu + d_x(y, x)\omega \end{cases} \quad (42)$$

where to simplify the presentation we consider the mono input case (i.e.,  $m = 1$ ) and  $\omega$  is an unknown input which is assumed to be a locally bounded time function taking values in  $\mathbb{R}^{n_\omega}$  and  $d_y$  and  $d_x$  are locally Lipschitz function of appropriate dimension. We assume that the function  $h(x)$  is a quadratic function. Hence, this one can be written in the form

$$h(x) = Hx + \begin{bmatrix} x' H_1 x \\ \vdots \\ x' H_{n_y} x \end{bmatrix} \quad (43)$$

where for all  $i$  in  $\{1, \dots, n_y\}$ ,  $H'_i = H_i$  is in  $\mathbb{R}^{n_x \times n_x}$ .

A framework to design a robust control law for this system can be to follow the  $H_\infty$  design methodology (see [16]). In this context, we are looking for a control law that satisfies two distinct objectives:

- 1) The first one is to guarantee the asymptotic stability of the origin when the disturbance vanishes.
- 2) The second one is to guarantee a given attenuation level of a quadratic functional of the state and control in the  $L_2$  framework. More precisely, given a positive definite matrix  $Q$  in  $\mathbb{R}^{(n_x+n_y) \times (n_x+n_y)}$  and a positive real number  $\gamma$  (the attenuation level) we want to find a stabilizing feedback control law  $u = \alpha_o(y, x)$  such that the following inequality is satisfied for all  $t$  in  $\mathbb{R}_+$ :

$$\begin{aligned} & \int_0^t [(y(s), x(s))' Q (y(s), x(s)) + u(s)^2] ds \\ & \leq \gamma^2 \int_0^t |\omega(s)|^2 ds \end{aligned} \quad (44)$$

where  $(y(\cdot), x(\cdot))$  denotes the solution of system (42) initialized to the origin.

Solving this problem relies on the construction of a solution to a nonlinear Hamilton Jacobi Isac equality which can be difficult (or impossible) to solve (see [16]).

However, if we focuss on the linear approximation of system (42), then this problem can be solved locally. The first order approximation of system (42) is a linear system defined as

$$\begin{cases} \dot{y} = Ay + Hx + D_y\omega \\ \dot{x} = Fx + Gu + D_x\omega \end{cases}, D_y = d_y(0,0), D_x = d_x(0,0). \quad (45)$$

In compact form, this linear system can be rewritten as follows:

$$\dot{\chi} = F\chi + Gu + D\omega \quad \chi' = [y', x'].$$

In the linear context, the Hamilton Jacobi Isac equality is an algebraic equation defined as

$$SF + F'S + \frac{1}{\gamma}SDD'S - SGG'S + Q = 0 \quad (46)$$

where the solution  $S$  is a positive definite matrix in  $\mathbb{R}^{(n_x+n_y) \times (n_x+n_y)}$ , and a robust linear control for system (45) solving the disturbance attenuation problem as defined by inequality (44) for the linear approximation is given as

$$u = K_o[y, x]' = -G'S\chi. \quad (47)$$

However, this control law guarantees only local asymptotic stability of the origin of system (42). We may apply the design methodology given in Theorem 1 to design a global asymptotic stabilizing controller  $u = \alpha_o(y, x)$  such that its local behavior is exactly  $K_o$ .

We assume that the system (45) is controllable and the matrix  $A$  is skew symmetric. This yields that Assumption 1 and 3 are satisfied. Moreover, the  $x$  subsystem being linear, it yields that Assumption 2 and 4 are trivially satisfied. In this case, we may apply the procedure of Theorem 1 as described by the following four steps.

- 1) First, we choose a local prescribed behavior  $K_o$  by solving the HJB algebraic (46) for given tuning parameters  $Q$  and  $\gamma$ .
- 2) We solve the linear matrix inequality (14) to find a forwarding like matrix  $\mathcal{P}$  [see Theorem 1 (10)]. Note that this step is not guaranteed to succeed when  $n_y > 1$ . This gives us a stabilizing controller  $K_x$  for the  $x$ -subsystem (see (27)) and its associated Lyapunov matrix  $R_x$  [given in (18)].
- 3) Then, using this  $K_x$  and  $R_x$ , we give an explicit solution  $\mathcal{M}$  to the partial differential (33). As shown in Appendix D, in our particular context this one can simply be expressed as

$$\mathcal{M}(x) = Mx + \begin{bmatrix} x'M_1x \\ \vdots \\ x'M_{n_y}x \end{bmatrix} \quad (48)$$

where  $M$  is solution to the Sylvester equation

$$M[F + GK_x] - AM = H \quad (49)$$

and  $(M_1, \dots, M_{n_y})$  are matrices in  $\mathbb{R}^{n_x \times n_x}$  obtained by solving the *unsquare* Sylvester equation<sup>7</sup>

$$\begin{aligned} [I_{n_y} \otimes [F + GK_x]' - A \otimes I_{n_x}] \cdot \begin{bmatrix} M_1 \\ \vdots \\ M_{n_y} \end{bmatrix} \\ + \begin{bmatrix} M_1 \\ \vdots \\ M_{n_y} \end{bmatrix} \cdot [F + GK_x] = \begin{bmatrix} H_1 \\ \vdots \\ H_{n_y} \end{bmatrix} \end{aligned} \quad (50)$$

where the operator  $\otimes$  is the Kronecker tensor product.

- 4) Next we construct the globally stabilizing feedback law defined as

$$\alpha_g(y, x) = (K_x - 2G'R_x)x + 2[y - \mathcal{M}(x)]'P \frac{\partial \mathcal{M}}{\partial x}(x)G \quad (51)$$

and we modify this, control law to match the local desired behavior. To complete the modified forwarding procedure, we construct a control law  $\alpha_o(y, x)$  [see (41)] with function  $\rho(y, x)$  chosen as

$$\rho(y, x) = \begin{cases} 0 & \text{if } [y' \quad x'] \mathcal{P} [yx] \leq \frac{1}{3}R_L, \\ \frac{3}{R_L} [y' \quad x'] \mathcal{P} [yx] - 1 & \text{if } \frac{1}{3}R_L \leq [y' \quad x'] \mathcal{P} [yx] \leq \frac{2}{3}R_L, \\ 1 & \text{if } [y' \quad x'] \mathcal{P} [yx] \geq \frac{2}{3}R_L \end{cases} \quad (52)$$

where  $R_L$  is computed with Lemma 4.

The benchmark example [10], (39), (see also [11]) fits in the class of system considered in this section. More precisely, system (42) is studied in the particular cases in which  $n_y = 1$ ,  $n_x = 2$  and the parameters are selected as follows:

$$\begin{aligned} A = 0, H_1 = \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}, H = [1 \quad 0], \\ F = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, G = D_x = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, D_y = 0. \end{aligned} \quad (53)$$

For this system we can follow the procedure to design a global stabilizer with local optimality.

- 1) We select the tuning parameter of the local optimal controller as

$$Q = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 10 \end{bmatrix}, \quad \gamma \approx 1.00.$$

Solving the associated Riccati equation (see (46)) by employing the routine (*care*) of Matlab with the attenuation level  $\gamma \approx 1.00$ , it yields the local optimal controller

$$K_o \approx [-4 \quad -24 \quad -71].$$

- 2) In the case  $n_y = 1$ , we obtain directly the matrix  $\mathcal{P}$  given as

$$\mathcal{P} \approx \begin{bmatrix} 6 & 17 & 24 \\ 17 & 80 & 147 \\ 24 & 147 & 426 \end{bmatrix}.$$

<sup>7</sup>It is shown in Appendix D that this Sylvester equation admits a solution.



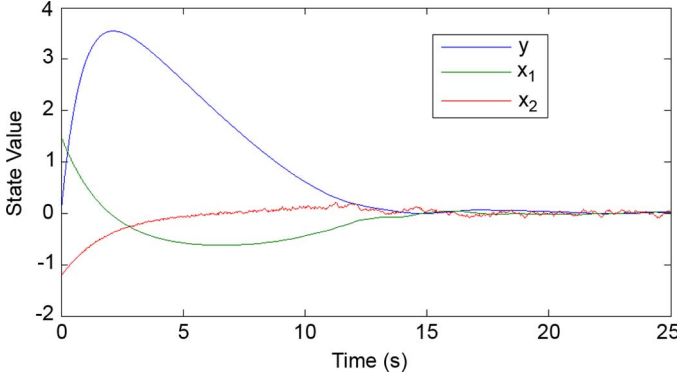


Fig. 1. Example of a closed loop trajectory.

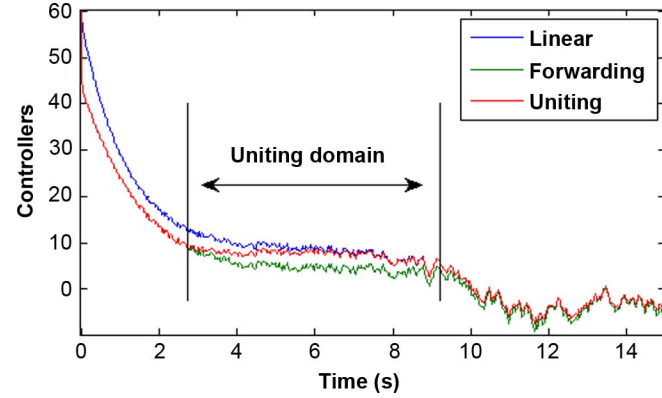


Fig. 2. Controllers.

This yields the controller  $K_x$  and the matrix  $R_x$  given as

$$K_x \approx \begin{bmatrix} -0.24 & -0.71 \end{bmatrix}, R_x \approx \begin{bmatrix} 5 & 13 \\ 13 & 54 \end{bmatrix}.$$

3) We get the solution to the PDE given in (48) with

$$M \approx \begin{bmatrix} -2.9 & -4 \end{bmatrix}, M_1 \approx \begin{bmatrix} -3.3 & -2 \\ -2 & -3.5 \end{bmatrix}.$$

4) By a Matlab computation, it yields the positive real number  $R_L$  given as

$$R_L \approx 5.$$

In the following figures is considered simulation of this control law when considering  $\omega$  to be a gaussian white noise with variance 2.

In Fig. 1 is shown a state trajectory when considering a particular initial condition for the disturbed model.

In Fig. 2 is depicted the associated control law. The red one is the locally optimal control. The blue is the evaluation of the optimal local and linear control law along the solution of the system. Finally the green one is the evaluation of the global forwarding control law. It can be checked that the solution goes from the green toward the red one when the solution gets close to the origin.

Fig. 3 compares the proposed control law which is locally optimal with respect to a given cost and the control law given in [10], (39), when considering solution initiated from the origin.

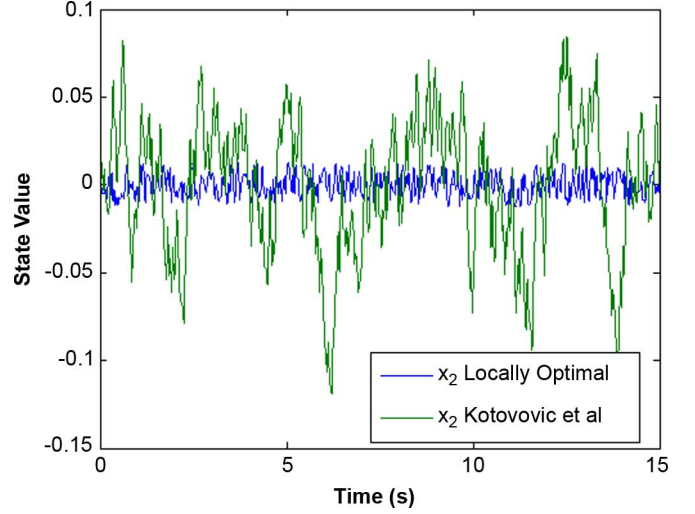


Fig. 3. Comparison with the controller of [10, Equation (39)].

#### IV. CONCLUSION

We have studied the problem of designing a stabilizing controller which ensures a desired local behavior. We have shown that given a prescribed locally stabilizing control law, provided there exists a Lyapunov matrix with a specific structure, this stabilizing local behaviors can be reproduced when using the forwarding design technique developed in [4], [5]. This is made possible by modifying the forwarding design adequately. Note that when the  $y$  subsystem is of dimension 1, this result establishes that all stabilizing local behaviors can be reproduced. This result gives a theoretical justification of a statistical result given in [9].

#### APPENDIX

*On the Feasibility of the Weak Lyapunov Inequality:* In this Section, we study the feasibility of the weak Lyapunov inequality (10) when considering systems whose first order approximation is the system (15). Assume a stabilizing local controller  $K_o = [0, k_2, k_x]$  is given. Note that, the necessary and sufficient conditions to make  $u = k_2 y_2 + k_x x$  a globally and asymptotically stabilizing input are

$$k_2 < 0, k_x < 0. \quad (54)$$

First of all note that  $A = \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}$ . Let  $P = \begin{bmatrix} P_{11} & P_{12} \\ P_{12} & P_{22} \end{bmatrix}$  in  $\mathbb{R}^{2 \times 2}$  be a Lyapunov matrix which satisfies (5). Note that

$$PA + A'P = \begin{bmatrix} 2P_{12} & P_{22} - P_{11} \\ P_{22} - P_{11} & -2P_{12} \end{bmatrix} = 0.$$

Hence, this implies that  $P_{12} = 0$  and  $P_{22} = P_{11}$ . In other word, the only Lyapunov matrix which satisfies (5) are those which take the form  $P = pI_2$ . For a candidate Lyapunov matrix in the form (we have normalized with respect to  $p$ )

$$\mathcal{P} \triangleq \begin{pmatrix} 1 & 0 & q_1 \\ 0 & 1 & q_2 \\ q_1 & q_2 & r \end{pmatrix}$$

to, be positive definite, parameters  $q_1$ ,  $q_2$  and  $r$  must satisfy

$$r > q_1^2 + q_2^2.$$

Assume there exists  $k_2$  and  $k_x$  which satisfies (54) and such that there exists  $q_1$ ,  $q_2$  and  $r$  with  $q_1$  and  $q_2$  not equal to zero such that the weak Lyapunov inequality (10) is satisfied. Inequality (10) implies that the following matrix is non positive:

$$\begin{aligned} Q &\triangleq [\Psi' \mathcal{P} + \mathcal{P} \Psi'] \\ &= \begin{bmatrix} 0 & k_2 q_1 & q_2 + k_x q_1 \\ * & 2k_2 q_2 & -q_1 + k_2 r + 1 + k_x q_2 \\ * & * & 2q_2 + 2k_x r \end{bmatrix}. \end{aligned}$$

It implies that for all  $(v_1, v_2)$  in  $\mathbb{R}^2$ , we have

$$[v_1, v_2, 0] Q \begin{bmatrix} v_1 \\ v_2 \\ 0 \end{bmatrix} \leq 0 \Leftrightarrow k_2 q_1 v_2 v_1 - 2k_2 q_2 v_2^2 \leq 0.$$

Hence, this implies that  $q_1 = 0$ . Moreover for all  $(v_1, v_3)$  in  $\mathbb{R}^2$ , we have

$$\begin{aligned} [v_1, 0, v_3] Q \begin{bmatrix} v_1 \\ 0 \\ v_3 \end{bmatrix} &:= [v_1, 0, v_3] \\ &\begin{bmatrix} 0 & 0 & q_2 \\ * & 2k_2 q_2 & k_2 r + 1 + k_x q_2 \\ * & * & 2q_2 + 2k_x r \end{bmatrix} \begin{bmatrix} v_1 \\ 0 \\ v_3 \end{bmatrix} \leq 0 \end{aligned}$$

which means for all  $(v_1, v_3)$  in  $\mathbb{R}^2$

$$q_2 v_3 v_1 + (2q_2 + 2k_x r) v_3^2 \leq 0.$$

Hence,  $q_1 = q_2 = 0$  which contradicts the assertion.

*Proof of Lemma 2:* The proof of this Lemma is based on recent results obtained in [15]. Indeed, the design of the function  $V_x$  is obtained from the uniting of a quadratic local control Lyapunov function (denoted  $V_0$ ) and a global control Lyapunov function (denoted  $V_\infty$ ) obtained employing a converse Lyapunov theorem.

First of all, employing the converse Lyapunov theorem of Kurzweil [17], there exists a  $C^\infty$  function  $V_\infty : \mathbb{R}^n \rightarrow \mathbb{R}_+$  such that

$$\frac{\partial V_\infty}{\partial x}(x)[f(x) + g(x)\alpha_x(x)] < 0, \quad \forall x \neq 0.$$

On the other hand, with (20), the function  $V_0(x) = x' R_x x$  is such that

$$\frac{\partial V_0}{\partial x}(x)[F + GK_x]x < 0, \quad \forall x \neq 0.$$

Due to the fact that  $K_x$  satisfies (7) it yields that the matrix  $F + GK_x$  is the first order approximation of the  $x$ -subsystem in (2) with the control law  $u = \alpha_x(x)$ . Consequently, it implies that there exists a positive real number  $\epsilon_1$  such that

$$\frac{\partial V_0}{\partial x}(x)[f(x) + g(x)\alpha_x(x)] < 0, \quad \forall |x| \leq \epsilon_1.$$

Employing [15, Theorem 2.1], it yields the existence of a function  $V_x$  and a positive real number  $\epsilon_2$  such that

1) for all  $x$  in  $\mathbb{R}^n \setminus \{0\}$

$$\frac{\partial V_x}{\partial x}(x)[f(x) + g(x)\alpha_x(x)] < 0$$

2) for all  $x$  in  $\mathbb{R}^n$  such that  $|x| \leq \epsilon_2$ , we have

$$V_x(x) = V_0(x)$$

and consequently  $\mathcal{H}(V_x)(0) = 2R_x$ .

This conclude the proof of Lemma 2

*Proof of Lemma 4:* With Assumption 2, there exists a neighborhood of the origin in which the distribution  $\text{Vect}\{g_1(x), \dots, g_m(x)\}$  is regular, involutive and of constant dimension  $m$ . Employing Frobenius theorem [18, Theorem 1.4.1], we know there exists a neighborhood of the origin  $U \subset \mathbb{R}^{n_x}$  and a diffeomorphism  $\varphi = (\varphi_1, \dots, \varphi_{n_x}) : U \rightarrow \varphi(U)$  such that

$$\frac{\partial \varphi_i}{\partial x}(x)g_j(x) = 0, \quad m$$

$$+1 \leq i \leq n_x, \quad 1 \leq j \leq m, \quad \forall x \in U.$$

Let  $\psi : U \rightarrow \psi(U)$  be the diffeomorphism defined as  $(\partial\varphi/\partial x(0))^{-1}\varphi(x)$ . Note that we have  $\partial\psi/\partial x(0) = I_{n_x}$ . Moreover, we have

$$G = g(0) = \left( \frac{\partial \varphi}{\partial x}(0) \right)^{-1} \begin{bmatrix} \frac{\partial \varphi_1}{\partial x}(0)g(0) \\ \vdots \\ \frac{\partial \varphi_m}{\partial x}(0)g(0) \\ 0 \\ \vdots \end{bmatrix}.$$

Hence, we get

$$\frac{\partial \psi}{\partial x}(x)g(x) = Gr(x), \quad \forall x \in U,$$

$$\text{where } r(x) = \begin{bmatrix} \frac{\partial \varphi_1}{\partial x}(0)g(0) \\ \vdots \\ \frac{\partial \varphi_m}{\partial x}(0)g(0) \end{bmatrix}^{-1} \begin{bmatrix} \frac{\partial \varphi_1}{\partial x}(x)g(x) \\ \vdots \\ \frac{\partial \varphi_m}{\partial x}(x)g(x) \end{bmatrix}.$$

If we denote the new coordinates  $\tilde{x} = \psi(x)$ , the system (2) takes the form

$$\dot{\tilde{x}} = \tilde{f}(\tilde{x}) + G\tilde{r}(\tilde{x})u \quad (55)$$

where  $\tilde{r}(\tilde{x})$  is a matrix in  $\mathbb{R}^{m \times m}$  for all  $\tilde{x}$  in  $\psi(U)$  and  $\tilde{r}(0) = I_m$ . Note that since  $\partial\psi/\partial x(0) = I_{n_x}$ , we have  $\partial\tilde{f}/\partial\tilde{x}(0) = F$ .

Consider now the Lyapunov function

$$V_L(y, x) = [y' \quad \psi(x)'] \mathcal{P} \begin{bmatrix} y \\ \psi(x) \end{bmatrix}.$$

We will show that this Lyapunov function is nonincreasing in a neighborhood of the origin when employing the control law  $u = \alpha_g(y, x)$ . Note that there exists  $a$  and  $b$  such that

$$\alpha_g(y, x) = a(\tilde{x}) + b(\tilde{x})y.$$

Note that we have the properties

$$\frac{\partial a}{\partial \tilde{x}}(0) = K_{g,x}, \quad b(0) = K_{g,y}.$$

When  $u = \alpha_g(y, x)$  the time derivative of the function  $V_L(y, x)$  satisfies along the trajectories of the nonlinear system (2)

$$\begin{aligned} \left. \dot{V}_L(y, x) \right|_{u=\alpha_g(y, x)} &= 2 \begin{bmatrix} y' & \tilde{x}' \end{bmatrix} \mathcal{P} \begin{bmatrix} Ay + \tilde{h}(\tilde{x}) \\ \tilde{f}(\tilde{x}) + G\tilde{r}(\tilde{x})\alpha_g(y, x) \end{bmatrix}. \end{aligned}$$

This gives

$$\begin{aligned} \left. \dot{V}_L(y, x) \right|_{u=\alpha_g(y, x)} &= 2 \begin{bmatrix} y' & \tilde{x}' \end{bmatrix} \mathcal{P} \left( \begin{bmatrix} A & H \\ GK_{g,y} & F + GK_{g,x} \end{bmatrix} \begin{bmatrix} y \\ \tilde{x} \end{bmatrix} \right. \\ &\quad \left. + \begin{bmatrix} \tilde{h}(\tilde{x}) - H\tilde{x} \\ \tilde{f}(\tilde{x}) - F\tilde{x} + G \left[ \tilde{r}(\tilde{x})(a(\tilde{x}) + b(\tilde{x})y) - K_g \begin{bmatrix} y \\ \tilde{x} \end{bmatrix} \right] \end{bmatrix} \right). \end{aligned}$$

Hence we get,

$$\begin{aligned} \left. \dot{V}_L(y, x) \right|_{u=\alpha_g(y, x)} &= \begin{bmatrix} y'QG & \tilde{x}' \end{bmatrix} \mathbb{M} \begin{bmatrix} G'Q'y \\ \tilde{x} \end{bmatrix} \\ &\quad + \Delta_1(\tilde{x}) + y'\Delta_2(\tilde{x}) + y'QG\Delta_3(\tilde{x})y \end{aligned} \quad (56)$$

where  $\mathbb{M}$  is the matrix defined in (57), as shown at the bottom of the page, where  $S_x$  is the negative definite matrix defined in (29). This matrix satisfies  $\mathbb{M} < -c_{\mathbb{M}}I_{n_x+1}$  where  $c_{\mathbb{M}} = \lambda_{\max}\{\mathbb{M}\}$  is a positive real number. Moreover we have

$$\begin{aligned} \Delta_1(\tilde{x}) &= 2 \begin{bmatrix} 0 & \tilde{x}' \end{bmatrix} \mathcal{P} \begin{bmatrix} \tilde{h}(\tilde{x}) - H\tilde{x} \\ \tilde{f}(\tilde{x}) - F\tilde{x} + G[\tilde{r}(\tilde{x})a(\tilde{x}) - K_{g,x}\tilde{x}] \end{bmatrix} \\ \Delta_2(\tilde{x}) &= 2 \begin{bmatrix} 1 & 0 \end{bmatrix} \mathcal{P} \begin{bmatrix} \tilde{h}(\tilde{x}) - H\tilde{x} \\ \tilde{f}(\tilde{x}) - F\tilde{x} + G[\tilde{r}(\tilde{x})a(\tilde{x}) - K_{g,x}\tilde{x}] \end{bmatrix} \\ &\quad + \left( \begin{bmatrix} 0 & \tilde{x}' \end{bmatrix} \mathcal{P} \begin{bmatrix} 0 \\ G[\tilde{r}(\tilde{x})b(\tilde{x}) - K_{g,y}] \end{bmatrix} \right)' \\ \Delta_3(\tilde{x}) &= 2\tilde{r}(\tilde{x})b(\tilde{x}) - K_{g,y}. \end{aligned}$$

Moreover, we have

$$|y'QG\Delta_3(\tilde{x})y| \leq \frac{|y'QG|^2 + |\Delta_3(\tilde{x})|^2}{2} |y|. \quad (58)$$

Hence, (56) becomes

$$\begin{aligned} \left. \dot{V}_L(y, x) \right|_{u=\alpha_g(y, x)} &\leq \\ &- |\tilde{x}|^2 \left( c_{\mathbb{M}} - \frac{\Delta_1(\tilde{x})}{|\tilde{x}|^2} - |y| \frac{|\Delta_2(\tilde{x})| + \frac{1}{2}|\Delta_3(\tilde{x})|^2}{|\tilde{x}|^2} \right) \\ &- |G'Q'y|^2 \left( c_{\mathbb{M}} - \frac{1}{2}|y| \right). \end{aligned} \quad (59)$$

Note that

$$\begin{aligned} |\Delta_1(\tilde{x})| &= O(|\tilde{x}|^3), \quad |\Delta_2(\tilde{x})| \\ &= O(|\tilde{x}|^2), \quad |\Delta_3(\tilde{x})| = O(|\tilde{x}|). \end{aligned}$$

Hence, this implies that there exists a positive real number  $R_g$  such that when  $u = \alpha_g(y, x)$  we get along the solutions of the system (2) for all  $(x, y)$  such that  $V_L(y, x) \leq R_g$

$$\left. \dot{V}_L(y, x) \right|_{u=\alpha_g(y, x)} \leq -\frac{c_{\mathbb{M}}}{2} [|\tilde{x}|^2 + |y'PMG|^2].$$

With the same analysis, it is possible to find a positive real number  $R_l$  such that by taking  $u = K_{o,y}y + K_{o,x}x$  we get a positive real number  $c_o$  such along the trajectories of the closed loop system we have for all  $(x, y)$  such that  $V_L(y, x) \leq R_l$

$$\left. \dot{V}_L(y, x) \right|_{u=K_{o,y}y+K_{o,x}x} \leq -c_o [|\tilde{x}|^2 + |y'PMG|^2].$$

Note that since  $\psi$  is a diffeomorphism, we get the existence of a positive real number such  $c_\psi$  that around the origin  $|\tilde{x}| \geq c_\psi|x|$ . Hence, we get the result with  $R_L = \min\{R_l, R_g\}$ .

*Solving the PDE for the Illustrative Example:* In this section we show that given, a vector  $K_x \in \mathbb{R}^{n_x}$  such that  $F + GK_x$  is Hurwitz the following partial differential equation:

$$\frac{\partial \mathcal{M}}{\partial x}(x)[F + GK_x]x = A\mathcal{M}(x) + h(x), \quad \forall x \in \mathbb{R}^n \quad (60)$$

can be solved explicitly when the function  $h$  is the quadratic function defined in (43).

First of all, note that following (32), the solution  $\mathcal{M} : \mathbb{R}^{n_x} \rightarrow \mathbb{R}^{n_y}$  can be expressed as:

$$\mathcal{M}(x) = \int_{-\infty}^0 \exp(-As)h\left(\exp\left([F + GK_x]s\right)x\right)ds. \quad (61)$$

The function  $h$  being quadratic, this implies that the function  $\mathcal{M}$  is also quadratic and may be written in the form (48) with  $(M, M_1, \dots, M_{n_y})$  are matrices in  $\mathbb{R}^{n_x \times n_x}$  to be selected. Assume for the time being that there exist solutions to the two

$$\mathbb{M} = \begin{bmatrix} -4 & -4(G'M'PM + G'R_x) \\ -4(R_xG + M'PMG) & S_x - 4(G'M'PM + R_xG')(GR_x + M'PMG) \end{bmatrix} \quad (57)$$

Sylvester (49) and (50) and let  $(M, M_1, \dots, M_{n_y})$  be these solutions. Note that we have

$$\frac{\partial \mathcal{M}}{\partial x}(x)[F + GK_x]x = [I_{n_y} \otimes x'] \Psi + M[F + GK_x]x$$

where  $\Psi$  is the matrix in  $\mathbb{R}^{(n_y n_x) \times n_x}$  defined by

$$\Psi = \begin{bmatrix} M_1(F + GK_x) + (F + GK_x)'M_1 \\ \vdots \\ M_{n_y}(F + GK_x) + (F + GK_x)'M_{n_y} \end{bmatrix}.$$

However, employing the fact that  $[M_1, \dots, M_{n_y}]'$  is solution to the Sylvester (50), we get

$$\begin{aligned} \Psi &= [I_{n_y} \otimes [F + GK_x]'] \begin{bmatrix} M_1 \\ \vdots \\ M_{n_y} \end{bmatrix} \\ &\quad + \begin{bmatrix} M_1 \\ \vdots \\ M_{n_y} \end{bmatrix} [F + GK_x] + \begin{bmatrix} H_1 \\ \vdots \\ H_{n_y} \end{bmatrix} \\ &= [A \otimes I_{n_x}] \begin{bmatrix} M_1 \\ \vdots \\ M_{n_y} \end{bmatrix} + \begin{bmatrix} H_1 \\ \vdots \\ H_{n_y} \end{bmatrix}. \end{aligned}$$

Hence, it implies

$$\begin{aligned} \frac{\partial \mathcal{M}}{\partial x}(x)[F + GK_x]x &= [I_{n_y} \otimes x'] [A \otimes I_{n_x}] \begin{bmatrix} M_1 \\ \vdots \\ M_{n_y} \end{bmatrix} x + [I_{n_y} \otimes x'] \begin{bmatrix} H_1 \\ \vdots \\ H_{n_y} \end{bmatrix} x \\ &\quad + AMx + Hx \end{aligned}$$

where we have used the fact that  $M$  satisfies the Sylvester (49). Employing the fact that

$$[I_{n_y} \otimes x'] [A \otimes I_{n_x}] \begin{bmatrix} M_1 \\ \vdots \\ M_{n_y} \end{bmatrix} = A \begin{bmatrix} x'M_1 \\ \vdots \\ x'M_{n_y} \end{bmatrix}$$

it yields

$$\begin{aligned} \frac{\partial \mathcal{M}}{\partial x}(x)[F + GK_x]x &= A \begin{bmatrix} x'M_1 \\ \vdots \\ x'M_{n_y} \end{bmatrix} x + AMx + Hx \\ &\quad + [I_{n_y} \otimes x'] \begin{bmatrix} H_1 \\ \vdots \\ H_{n_y} \end{bmatrix} x \\ &= A\mathcal{M}(x) + h(x). \end{aligned}$$

Consequently, if  $(M, M_1, \dots, M_{n_y})$  are matrices in  $\mathbb{R}^{n_x \times n_x}$  solution to the Sylvester (49) and (50) the function  $\mathcal{M}$  defined in (48) is solution to the PDE (60).

It remains to show that the two Sylvester (49) and (50) admit a solution. Note that for the first one [i.e., (49)], this is trivial since the two matrices  $F + GK_x$  and  $-A$  have different eigenvalues ( $F + GK_x$  is Hurwitz and  $A$  is stable).

The same property holds for (50). Indeed, with the matrix  $R_x$  given in (18), we have

$$\begin{aligned} &(I_{n_y} \otimes R_x) [I_{n_y} \otimes [F + GK_x] - A' \otimes I_{n_x}] \\ &\quad + [I_{n_y} \otimes [F + GK_x]' - A \otimes I_{n_x}] (I_{n_y} \otimes R_x) \\ &= I_{n_y} \otimes (R_x[F + GK_x] + [F + GK_x]'R_x) \\ &\quad - (I_{n_y} \otimes R_x)(A' \otimes I_{n_x}) - (A \otimes I_{n_x})(I_{n_y} \otimes R_x). \end{aligned}$$

Note that we have

$$\begin{aligned} (I_{n_y} \otimes R_x)(A' \otimes I_{n_x}) + (A \otimes I_{n_x})(I_{n_y} \otimes R_x) \\ = A' \otimes R_x + A \otimes R_x = 0 \end{aligned}$$

since, by assumption,  $A' = -A$ . Consequently, it implies with (20)

$$\begin{aligned} &(I_{n_y} \otimes R_x) [I_{n_y} \otimes [F + GK_x] - A' \otimes I_{n_x}] \\ &\quad + [I_{n_y} \otimes [F + GK_x]' - A \otimes I_{n_x}] (I_{n_y} \otimes R_x) \\ &= I_{n_y} \otimes (R_x[F + GK_x] + [F + GK_x]'R_x) < 0 \end{aligned}$$

which is a Lyapunov equality with Lyapunov matrix  $(I_{n_y} \otimes R_x)$ . Hence, it establishes that the matrix  $[I_{n_y} \otimes [F + GK_x] - A' \otimes I_{n_x}]$  is Hurwitz and has different eigenvalues with the matrix  $-\bar{F} + GK_x$ .

## REFERENCES

- [1] M. Krstic, I. Kanellakopoulos, and P. Kokotovic, *Nonlinear and Adaptive Control Design*. New York, NY, USA: Wiley, 1995.
- [2] V. Andrieu and L. Praly, "Global asymptotic stabilization for nonminimum phase nonlinear systems admitting a strict normal form," *IEEE Trans. Autom. Control*, vol. 53, no. 5, pp. 1120–1132, May 2008.
- [3] A. R. Teel, "A nonlinear small gain theorem for the analysis of control systems with saturation," *IEEE Trans. Autom. Control*, vol. 41, no. 9, pp. 1256–1270, Sep. 1996.
- [4] F. Mazenc and L. Praly, "Adding integrations, saturated controls, and stabilization for feedforward systems," *IEEE Trans. Autom. Control*, vol. 41, no. 11, pp. 1559–1578, Nov. 1996.
- [5] M. Jankovic, R. Sepulchre, and P. Kokotovic, "Constructive Lyapunov stabilization of nonlinear cascade systems," *IEEE Trans. Autom. Control*, vol. 41, no. 12, pp. 1723–1735, Dec. 1996.
- [6] L. Praly, R. Ortega, and G. Kaliora, "Stabilization of nonlinear systems via forwarding mod  $\{L_1 \text{ sub}_? g_1 / \text{sub}_? V\}$ ," *IEEE Trans. Autom. Control*, vol. 46, no. 9, pp. 1461–1466, Sep. 2002.
- [7] P. Kokotovic and M. Arcak, "Constructive nonlinear control: a historical perspective," *Automatica*, vol. 37, no. 5, pp. 637–662, 2001.
- [8] Z. Pan, K. Ezal, A. Krener, and P. Kokotovic, "Backstepping design with local optimality matching," *IEEE Trans. Autom. Control*, vol. 46, no. 7, pp. 1014–1027, Jul. 2001.
- [9] M. Sahnoun, V. Andrieu, and M. Nadri, "Nonlinear and locally optimal controllers design for input affine locally controllable systems," *Int. J. Control*, vol. 85, no. 2, pp. 159–170, 2012.
- [10] R. Sepulchre, M. Jankovic, and P. Kokotovic, "Integrator forwarding: a new recursive nonlinear robust design," *Automatica*, vol. 33, no. 5, pp. 979–984, 1997.
- [11] D. Carnevale and A. Astolfi, "Integrator forwarding without PDES," in *Proc. 48th IEEE Conf. Decision Control & 28th Chinese Control Conf. (CDC/CCC'09)*, 2009, pp. 33–38.
- [12] S. Benachour, V. Andrieu, L. Praly, and H. Hammouri, "Adding an integration with prescribed local behavior," in *Proc. 50th IEEE Conf. Decision Control*, 2011, pp. 7555–7560.
- [13] R. Sepulchre, M. Jankovic, and P. V. Kokotovic, *Constructive Nonlinear Control, ser. Communications and Control Engineering Series*. New York: Springer-Verlag, 1997.
- [14] L. Praly, "Lyapunov functions, stability and stabilization," *Ecole Nationale Supérieure des Mines de Paris*, 2008.

- [15] V. Andrieu and C. Prieur, "Uniting two control Lyapunov functions for affine systems," *IEEE Trans. Autom. Control*, vol. 55, no. 8, pp. 1923–1927, Aug. 2010.
- [16] T. Basar and P. Bernhard, *H<sub>∞</sub>-Optimal Control and Related Minimax Design Problems: a Dynamic Game Approach*. Boston, MA: Birkhauser, 1995, vol. 5.
- [17] J. Kurzweil, "On the inversion of Lyapunov second theorem on stability of motion," *Annu. Math. Soc. Trans. Ser.*, vol. 2, no. 24, pp. 19–77, 1956.
- [18] A. Isidori, *Nonlinear Control Systems: an Introduction*. New York, NY, USA: Springer-Verlag, 1989.



**M<sup>ed</sup> Sofiane Benachour** (M'13) was born in Sétif, Algeria, in 1983. He graduated from École Nationale Préparatoire aux études d'ingénierat Rouiba Algeria in 2003, and received the engineer's degree in automatic control and electrical engineering from the Université Ferhat Abbas Sétif, Algeria, in 2007, the M.Res. degree in automatic mechatronics, aeronautics and spatial engineering from the Université de Bordeaux 1, Talence, France, and is currently pursuing the Ph.D. degree at the Université de Lyon 1, Villeurbanne, France.

His research interests include stability of nonlinear systems, Lyapunov design, theory and application of qualitative nonlinear control.



**Vincent Andrieu** (A'05) was born in Rouen, France, in 1978. He graduated in engineering and mathematics from INSA de Rouen and université de Rouen, France, in 2001 and received the Ph.D. degree from École des Mines de Paris, Paris, France, in 2005 for his work on output feedback and observer design for non linear systems.

In 2006, he went to Imperial College London, London, U.K., as a Research Assistant. In 2008, he has joined the CNRS-LAAS lab, Toulouse, France, as a CNRS-chargé de recherche. Since 2010, he has been with the LAGEP-CNRS, Université de Lyon 1. His main research interests are in feedback stabilization of controlled dynamical nonlinear systems and state estimation problem. He is also interested in practical application of these theoretical problems, and especially in the field of aeronautics.



**Laurent Praly** (M'07) graduated as an engineer from the École Nationale Supérieure des Mines de Paris, Paris, France, in 1976 and received the Ph.D. degree in automatic control and mathematics from the Université Paris IX Dauphine, in 1988.

After working in industry for three years, in 1980 he joined the Centre Automatique et Systèmes at École des Mines de Paris where he is currently. His main interest is in observers and feedback stabilization/regulation for controlled dynamical systems under various aspects—linear and nonlinear, dynamic, output, under constraints, with parametric or dynamic uncertainty, disturbance attenuation or rejection —. On these topics he is contributing both on the theoretical aspect with many academic publications and the practical aspect with applications in power systems, electric drives/mechanical systems, aerodynamical and space vehicles.



**Hassan Hammouri** received the Ph.D. degrees in mathematics from the University Joseph Fourier, Saint-Martin-d'Hères 38041, France, in 1983 and the D.Sc. degree in control from the Institut National Polytechnique de Grenoble, Grenoble, France, in 1991.

Since 1992, he has been a Professor of automatic control in the Department of Electrical and Chemical Engineering, University Lyon 1, Lyon, France. His research interests include stability of nonlinear systems, nonlinear observer, fault diagnosis, control of distributed parameter systems, and applications to control of Electrical, Chemical and Biological systems.