

Null controllability using flatness: a case study of a 1-D heat equation with discontinuous coefficients

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Abstract—The approach recently proposed by the authors for the null controllability of 1-D parabolic equations is applied to the nontrivial case of a heat equation with discontinuous coefficients and subjected to Robin boundary conditions. The control steering the system to zero from a discontinuous initial state is comprehensively derived, together with the corresponding trajectory. Numerical experiments illustrate several features of the theory and demonstrate its effectiveness.

I. INTRODUCTION

The null controllability of parabolic equations has been extensively investigated since several decades. After the pioneering works [1]–[3], mainly concerned with the 1-D case, there has been significant progress in the N-D case by using Carleman estimates, see in particular [4]. More recently, the case of discontinuous coefficients has been studied along similar lines [5]–[7]. A direct alternative approach based on the so-called flatness property [8], [9], was proposed in [10] for the plain heat equation, and extended to the parabolic case with fairly irregular coefficients [11].

In this paper we apply the method of [11] to a physically relevant problem with discontinuous coefficients. We consider the heat conduction in a one-dimensional rod made of two sections with constant thermal properties. Without restriction, we can assume the rod has length 1, with one section of length X and the other of length $1 - X$. The evolution of the temperature Θ is given by the heat equation

$$\rho \Theta_t(x, t) = (a \Theta_x)_x(x, t);$$

a and ρ are the piecewise constant functions on $(0, 1)$

$$(a(x), \rho(x)) := \begin{cases} (a_0, \rho_0), & 0 < x < X \\ (a_1, \rho_1), & X < x < 1, \end{cases}$$

where a_0, a_1, ρ_0, ρ_1 are strictly positive constants. This situation is typical of composite materials. At the 0-end the rod is submitted to the constant ambient temperature Θ_0 , and at the 1-end to a time-varying heat source (the control input) of temperature $\Theta_1(t)$. The heat flux $-a \Theta_x$ at the ends obeys the convection conditions

$$\begin{aligned} -(a \Theta_x)(0, t) &= h_0 (\Theta_0 - \Theta(0, t)) \\ -(a \Theta_x)(1, t) &= h_1 (\Theta(1, t) - \Theta_1(t)), \end{aligned}$$

with h_0 and h_1 positive constants. Setting $\theta(x, t) := \Theta(x, t) - \Theta_0$ and taking as the control input $u(t) := \Theta_1(t) - \Theta_0$ results

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in the boundary value problem

$$\rho \theta_t(x, t) - (a \theta_x)_x(x, t) = 0, \quad (x, t) \in (0, 1) \times (0, T) \quad (1)$$

$$\alpha_0 \theta(0, t) + \beta_0 (a \theta_x)(0, t) = 0 \quad (2)$$

$$\alpha_1 \theta(1, t) + \beta_1 (a \theta_x)(1, t) = u(t), \quad (3)$$

where the constants $\alpha_0, \beta_0, \alpha_1, \beta_1$ satisfy $\alpha_0^2 + \beta_0^2 > 0$, $\alpha_1^2 + \beta_1^2 > 0$, $\alpha_0 \beta_0 \leq 0$ and $\alpha_1 \beta_1 \geq 0$. Note the two limiting cases: $\beta_i = 0$ (Dirichlet condition), obtained when taking $h_i \rightarrow \infty$; $\alpha_i = 0$ (Neumann condition), obtained when considering the control input is $u(t) := h_1 (\Theta(1, t) - \Theta_1(t))$ and taking $h_0 = 0$. Included in the formulation of the system is the fact that a solution θ and its quasi-derivative $a \theta_x$ are differentiable in particular at $x = X$ (whereas θ_x will in general be discontinuous at X). We could thus rewrite (1) more explicitly as the piecewise constant heat equation

$$\begin{cases} \theta_t(x, t) = \frac{a_0}{\rho_0} \theta_{xx}(x, t), & 0 < x < X \\ \theta_t(x, t) = \frac{a_1}{\rho_1} \theta_{xx}(x, t), & X < x < 1 \end{cases}$$

together with the so-called interface conditions

$$\begin{aligned} \theta(X^-, t) &= \theta(X^+, t) \\ a_0 \theta_x(X^-, t) &= a_1 \theta_x(X^+, t). \end{aligned}$$

The aim of this paper is to fully derive and numerically test the open-loop control steering the system (1)–(3) from an initial state $\theta_0 \in L^2(0, 1)$ at time 0 to the final state 0 at time T . We follow the approach proposed in [11] for the null controllability of general 1-D parabolic equations with fairly irregular coefficients. The paper runs as follows: in section II, we recall the main formal steps of the approach on our specific example; in section III, we give the detailed expressions of the quantities involved in the control law; finally in section IV, we present detailed numerical experiments.

II. OUTLINE OF THE FLATNESS-BASED APPROACH

In [11] is established a general result for the null controllability of the one-dimensional parabolic system

$$\begin{aligned} \rho \theta_t - (a \theta_x)_x - b \theta_x - c \theta &= 0, \quad (x, t) \in (0, 1) \times (0, T) \\ \alpha_0 \theta(0, t) + \beta_0 (a \theta_x)(0, t) &= 0 \\ \alpha_1 \theta(1, t) + \beta_1 (a \theta_x)(1, t) &= u(t), \end{aligned}$$

where a, b, c, ρ are functions on $(0, 1)$ such that;

- $a(x) > 0$ and $\rho(x) > 0$ for almost all $x \in (0, 1)$
- $\exists K \geq 0$ such that $c(x) \leq K \rho(x)$ for almost all $x \in (0, 1)$.

Theorem 1: Assume $\frac{1}{a}, \frac{b}{a}, c, \rho \in L^1(0, 1)$ and $a^{1-\frac{1}{p}} \rho \in L^p(0, 1)$ for some $p \in (1, \infty]$. Consider an initial state $\theta_0 \in L^1(0, 1)$, a final time $T > 0$ and $s \in (1, 2 - \frac{1}{p})$.

Then there exists a control $u \in G^s([0, T], \mathbb{R})$ which steers the system from θ_0 to the final state $\theta(\cdot, T) = 0$. Moreover $\theta, a\theta_x \in G^s([\varepsilon, T], W^{1,1}(0, 1))$ for all $\varepsilon \in (0, T)$.

In the theorem, $L_\rho^1(0, 1)$ is the space of functions f such that $\int_0^1 |f(x)|\rho(x)dx < \infty$; $G^s([0, T], B) \subset C^\infty([0, T], B)$, where B is a Banach space with norm $\|\cdot\|_B$, is the class of Gevrey functions of order s , i.e. such that for some $M, R > 0$,

$$\|y^{(i)}(t)\|_B \leq M \frac{i!^s}{R^i}, \quad \forall t \in [0, T], \quad \forall i \geq 0.$$

The proof of this result provides an explicit construction of the control u in the form of an infinite series. We outline in the sequel the formal aspects of the construction for our particular case (1)–(3), where $b = c = 0$; also $\frac{1}{a}, \rho \in L^\infty(0, 1)$, which implies $L^2(0, 1) \subset L_\rho^1(0, 1)$. We refer the reader to [11] for all the technical aspects, in particular proofs of convergence of all the series appearing in the sequel. The method comprises two phases: we first apply a zero control on $[0, \tau]$, where $\tau \in (0, T)$ is some arbitrary intermediate time, to steer the system from the “irregular” initial state $\theta_0 \in L^2$ to a “more regular” intermediate state θ_τ ; we then use the flatness property to steer the system from θ_τ to the final state $\theta(T, x) = 0$.

A. First phase: null control on $[0, \tau]$

Since $u(t) = 0$ here, the boundary condition (3) becomes

$$\alpha_1 \theta(1, t) + \beta_1 (a\theta_x)(1, t) = 0, \quad (4)$$

and we can solve (1), (2) and (4) by the method of separation of variables. Indeed, there exists an orthonormal basis $(e_n)_{n \geq 0}$ of $L_\rho^2(0, 1)$ and a sequence $(\lambda_n)_{n \geq 0}$ in \mathbb{R} such that

$$-(ae'_n)' = \lambda_n \rho e_n \quad (5)$$

$$\alpha_0 e_n(0) + \beta_0 (ae'_n)(0) = 0 \quad (6)$$

$$\alpha_1 e_n(1) + \beta_1 (ae'_n)(1) = 0. \quad (7)$$

$L_\rho^2(0, 1)$ is the space of functions f such that $\langle f, f \rangle_\rho < \infty$, endowed with the inner product $\langle f, g \rangle_\rho := \int_0^1 f(x)g(x)\rho(x)dx$. In our case $L^2(0, 1) = L_\rho^2(0, 1)$ since ρ and $\frac{1}{\rho}$ are bounded.

In other words, the λ_n 's and e_n 's are the eigenvalues and eigenfunctions of the Sturm-Liouville problem

$$-(a\phi')' = \lambda \rho \phi \quad (8)$$

$$\alpha_0 \phi(0) + \beta_0 (a\phi')(0) = 0 \quad (9)$$

$$\alpha_1 \phi(1) + \beta_1 (a\phi')(1) = 0. \quad (10)$$

As we will need this fact in section III-B, we now prove the λ_n 's are strictly positive (and by the way rederive that the λ_n 's, hence the e_n 's, are real). Indeed, consider a (possibly complex) solution λ, ϕ of (8)–(10). On the one hand by (8),

$$\int_0^1 \bar{\phi}(x)(a\phi')'(x)dx = -\lambda \int_0^1 |\phi(x)|^2 \rho(x)dx,$$

where $\bar{\phi}$ is the complex conjugate of ϕ ; on the other hand, integrating (8) by parts gives

$$\begin{aligned} \int_0^1 \bar{\phi}(x)(a\phi')'(x)dx &= [(a\phi'\bar{\phi})(x)]_0^1 - \int_0^1 (a\phi'\bar{\phi}')dx \\ &= K_0 - K_1 - \int_0^1 a(x)|\phi'(x)|^2 dx, \end{aligned}$$

where $K_i := \alpha_i \beta_i \frac{|\phi(i)|^2 + |(a\phi')(i)|^2}{\alpha_i^2 + \beta_i^2}$. As a consequence,

$$\lambda \int_0^1 |\phi(x)|^2 dx = K_1 - K_0 + \int_0^1 a(x)|\phi'(x)|^2 dx,$$

which implies λ is real and, because $\alpha_0 \beta_0 \leq 0$ and $\alpha_1 \beta_1 \geq 0$, strictly positive.

As $(e_n)_{n \geq 0}$ is an orthonormal basis of $L_\rho^2(0, 1)$, we can expand the initial condition as $\theta_0 = \sum_{n \geq 0} c_n e_n$ in $L_\rho^2(0, 1)$, with coefficients $c_n := \langle \theta_0, e_n \rangle_\rho$ such that $\sum_{n \geq 0} |c_n|^2 < \infty$. It is then easy to check that

$$\theta(x, t) := \sum_{n \geq 0} c_n e^{-\lambda_n t} e_n(x)$$

is the solution of (1), (2), (4) for $t \in (0, \tau]$ starting from θ_0 .

B. Second phase: flatness-based control on $[\tau, T]$

We now show the state $\theta_\tau(x) := \theta(x, \tau)$ reached at the end of the first phase can be steered to 0. To this end, we now seek θ in the form

$$\theta(x, t) := \sum_{i \geq 0} g_i(x) y^{(i)}(t), \quad (11)$$

where the generating functions g_i are solutions of the sequence of Cauchy problems

$$(ag'_0)' = 0 \quad (12)$$

$$\alpha_0 g_0(0) + \beta_0 (ag'_0)(0) = 0 \quad (13)$$

$$\beta_0 g_0(0) - \alpha_0 (ag'_0)(0) = K \quad (14)$$

for some $K \neq 0$, and

$$(ag'_i)' = \rho g_{i-1} \quad (15)$$

$$\alpha_0 g_i(0) + \beta_0 (ag'_i)(0) = 0 \quad (16)$$

$$\beta_0 g_i(0) - \alpha_0 (ag'_i)(0) = 0 \quad (17)$$

for $i \geq 0$. It can then be shown that for some $C, R > 0$

$$\sup_{x \in [0, 1]} |g_i(x)| \leq \frac{C}{R^i (i!)^2}, \quad \forall i \geq 0,$$

so that the series (11) converges as soon as $y \in G^s([\tau, T], \mathbb{R})$ with $s < 2$.

On the other hand, each eigenfunction e_n can be expanded on the g_i 's as $e_n = \zeta_n \sum_{i \geq 0} (-\lambda_n)^i g_i$, with

$$\zeta_n := \frac{\beta_0 e_n(0) - \alpha_0 (ae'_n)(0)}{\beta_0 g_0(0) - \alpha_0 (ag'_0)(0)}.$$

Indeed, setting $f_n := \zeta_n \sum_{i \geq 0} (-\lambda_n)^i g_i$ we find

$$\begin{aligned} (af'_n)' &= \zeta_n \sum_{i \geq 0} (-\lambda_n)^i (ag'_i)' \\ &= \zeta_n \sum_{i \geq 1} (-\lambda_n)^i (\rho g_{i-1}) \\ &= -\lambda_n \rho \zeta_n \sum_{j \geq 0} (-\lambda_n)^j g_j \\ &= -\lambda_n \rho f_n \end{aligned}$$

$$\alpha_0 f_n(0) + \beta_0 (af'_n)(0) = \zeta_n (\alpha_0 g_0(0) + \beta_0 (ag'_0)(0)) = 0$$

$$\beta_0 f_n(0) - \alpha_0 (af'_n)(0) = \zeta_n (\beta_0 g_0(0) - \alpha_0 (ag'_0)(0))$$

$$= \beta_0 e_n(0) - \alpha_0 (ae'_n)(0).$$

Therefore $e_n - f_n$ satisfies a Cauchy problem with zero initial conditions, implying $e_n - f_n = 0$.

It is now easy to check that the control defined by

$$y(t) := \phi_s \left(\frac{t - \tau}{T - \tau} \right) \sum_{n \geq 0} c_n \zeta_n e^{-\lambda_n t} \quad (18)$$

$$u(t) := \sum_{i \geq 0} (\alpha_i g_i(1) + \beta_i g_i'(1)) y^{(i)}(t), \quad (19)$$

where ϕ_s is the ‘‘Gevrey step’’ of section III-C, steers the system from θ_τ at time τ to 0 at time T . Indeed, (11), (18), (19) is clearly the solution of (1)–(3); as $\phi_s^{(i)}(1) = 0$ for $i \geq 0$,

$$\theta(T, x) = \sum_{i \geq 0} y^{(i)}(T) g_i(x) = 0;$$

and as $\phi_s(0) = 1$ and $\phi_s^{(i)}(0) = 0$ for $i \geq 1$,

$$\begin{aligned} \theta_\tau(x) &= \sum_{n \geq 0} c_n e^{-\lambda_n \tau} e_n(x) \\ &= \sum_{n \geq 0} c_n e^{-\lambda_n \tau} \zeta_n \sum_{i \geq 0} (-\lambda_n)^i g_i(x) \\ &= \sum_{i \geq 0} \left(\sum_{n \geq 0} c_n \zeta_n e^{-\lambda_n \tau} (-\lambda_n)^i \right) g_i(x) \\ &= \sum_{i \geq 0} y^{(i)}(\tau) g_i(x). \end{aligned}$$

III. EXPLICIT EXPRESSIONS

We now provide explicit expressions for the generating functions g_i , the eigenfunctions e_n and the derivatives of the ‘‘Gevrey step’’ ϕ_s . We set $\kappa_0 := \sqrt{\frac{\rho_0}{a_0}}$ and $\kappa_1 := \sqrt{\frac{\rho_1}{a_1}}$.

A. Generating functions

It is easily seen that the solution of (12)–(17) is

$$g_i(x) = \begin{cases} g_{i,0}(x), & 0 < x < X \\ g_{i,1}(x), & X < x < 1, \end{cases}$$

where

$$\begin{aligned} g_{i,0}(x) &= K \left(a_0 \beta_0 - \frac{\alpha_0 x}{2i+1} \right) \frac{(\kappa_0 x)^{2i}}{(2i)!} \\ g_{i,1}(x) &= \sum_{j=0}^i \left[g_{i-j,0}(X) + \frac{a_0}{a_1} \frac{(x-X) g'_{i-j,0}(X)}{2j+1} \right] \frac{(\kappa_1 (x-X))^{2j}}{(2j)!}. \end{aligned}$$

The quasiderivatives are $(ag'_{0,0})(x) = (ag'_{0,1})(x) = -a_0 K \alpha_0$, and for $i \geq 1$,

$$\begin{aligned} (ag'_{i,0})(x) &= a_0 \kappa_0 K \left(a_0 \beta_0 - \frac{\alpha_0 x}{2i} \right) \frac{(\kappa_0 x)^{2i-1}}{(2i-1)!} \\ (ag'_{i,1})(x) &= (ag'_{i,0})(x) + \kappa_1 \sum_{j=1}^i \left[a_1 g_{i-j,0}(X) \right. \\ &\quad \left. + \frac{(x-X)(ag'_{i-j,0}(X))}{2j} \right] \frac{(\kappa_1 (x-X))^{2j-1}}{(2j-1)!}. \end{aligned}$$

Clearly, the initial conditions (13), (14), (16) and (17) are satisfied, as well as the interface conditions $g_{i,0}(X) = g_{i,1}(X)$ and $(ag'_{i,0})(X) = (ag'_{i,1})(X)$.

B. Eigenvalues and eigenfunctions

Since we have proved the Sturm-Liouville problem (8)–(10) may have nonzero solutions only for $\lambda > 0$, we set $\mu := \sqrt{\lambda}$. A candidate solution ϕ then reads

$$\phi(x) = \begin{cases} \phi_0(x), & 0 < x < X \\ \phi_1(x), & X < x < 1, \end{cases}$$

with

$$\begin{aligned} \phi_0(x) &= C_0 \cos(\mu \kappa_0 x) + D_0 \sin(\mu \kappa_0 x) \\ \phi_1(x) &= C_1 \cos(\mu \kappa_1 (x-X)) + D_1 \sin(\mu \kappa_1 (x-X)). \end{aligned}$$

The interface conditions $\phi_0(X) = \phi_1(X)$ and $(a\phi_0)'(X) = (a\phi_1)'(X)$ then yield (using $\mu \neq 0$)

$$C_1 = C_0 \cos(\mu \kappa_0 X) + D_0 \sin(\mu \kappa_0 X) \quad (20)$$

$$D_1 = \frac{a_0 \kappa_0}{a_1 \kappa_1} (D_0 \cos(\mu \kappa_0 X) - C_0 \sin(\mu \kappa_0 X)). \quad (21)$$

The boundary conditions (9), (10) read

$$\alpha_0 C_0 + \beta_0 \mu \kappa_0 D_0 = 0 \quad (22)$$

$$(\alpha_1 c_1 - \mu \beta_1 a_1 \kappa_1 s_1) C_1 + (\alpha_1 s_1 + \mu \beta_1 a_1 \kappa_1 c_1) D_1 = 0, \quad (23)$$

where we have set

$$\begin{aligned} c_0 &:= \cos(\mu \kappa_0 X) \\ s_0 &:= \sin(\mu \kappa_0 X) \\ c_1 &:= \cos(\mu \kappa_1 (1-X)) \\ s_1 &:= \sin(\mu \kappa_1 (1-X)). \end{aligned}$$

Injecting (20), (21) into (22), (23) gives the linear system

$$\begin{pmatrix} \alpha_0 & \beta_0 \mu \kappa_0 \\ F(\mu) & G(\mu) \end{pmatrix} \begin{pmatrix} C_0 \\ D_0 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix},$$

which has a nonzero solution iff the determinant $f(\mu) := \alpha_0 G(\mu) - \beta_0 \mu \kappa_0 F(\mu)$ is zero. Since

$$\begin{aligned} f(\mu) &= (\alpha_0 \alpha_1 + \mu^2 \beta_0 \beta_1 a_0 \rho_0) s_0 c_1 \\ &\quad + \left(\alpha_0 \alpha_1 \frac{a_0 \kappa_0}{a_1 \kappa_1} + \mu^2 \beta_0 \beta_1 a_0 \rho_0 \frac{a_1 \kappa_1}{a_0 \kappa_0} \right) c_0 s_1 \\ &\quad + \mu a_0 \kappa_0 \left[(\alpha_0 \beta_1 - \alpha_1 \beta_0) c_0 c_1 \right. \\ &\quad \left. - \left(\alpha_0 \beta_1 \frac{a_1 \kappa_1}{a_0 \kappa_0} - \alpha_1 \beta_0 \frac{a_0 \kappa_0}{a_1 \kappa_1} \right) s_0 s_1 \right] \end{aligned}$$

is odd, and $\mu = 0$ is excluded, we are interested only in the strictly positive roots of $f(\mu) = 0$. There is no closed-form expression for these roots, so they must be determined numerically. In the simulations of section IV, we have for instance used the function `roots` from the open-source package `Chebfun` [12], which is very handy to find all the roots of a function in a given interval.

To each strictly positive root μ_n of f then corresponds the eigenfunction

$$e_n(x) = \begin{cases} e_{n,0}(x), & 0 < x < X \\ e_{n,1}(x), & X < x < 1, \end{cases}$$

with

$$e_{n,0}(x) = M_n \left[\beta_0 a_0 \cos(\mu_n \kappa_0 x) - \alpha_0 \frac{\sin(\mu_n \kappa_0 x)}{\mu_n \kappa_0 x} \right]$$

$$e_{n,1}(x) = e_{n,0}(X) \cos(\mu_n \kappa_0 x) + \frac{a_0}{a_1} e'_{n,0}(X) \frac{\sin(\mu_n \kappa_1 (x - X))}{\mu_n \kappa_1};$$

the coefficient M_n is chosen so that $\langle e_n, e_n \rangle_\rho = 1$. The quasi-derivatives are

$$(ae'_{n,0})(x) = -M_n [\beta_0 a_0 \mu_n \kappa_0 \sin(\mu_n \kappa_0 x) + \alpha_0 \cos(\mu_n \kappa_0 x)]$$

$$(ae'_{n,1})(x) = -e_{n,0}(X) \mu_n \kappa_0 \sin(\mu_n \kappa_0 x)$$

$$+ \frac{1}{a_1} (ae'_{n,0})(X) \cos(\mu_n \kappa_1 (x - X)).$$

Clearly, the boundary conditions (6), (7) are satisfied, as well as the interface conditions $e_{n,0}(X) = e_{n,1}(X)$ and $(ae'_{n,0})(X) = (ae'_{n,1})(X)$.

Fig. 1 displays some eigenfunctions; though not obvious at first sight, these eigenfunctions are indeed orthogonal.

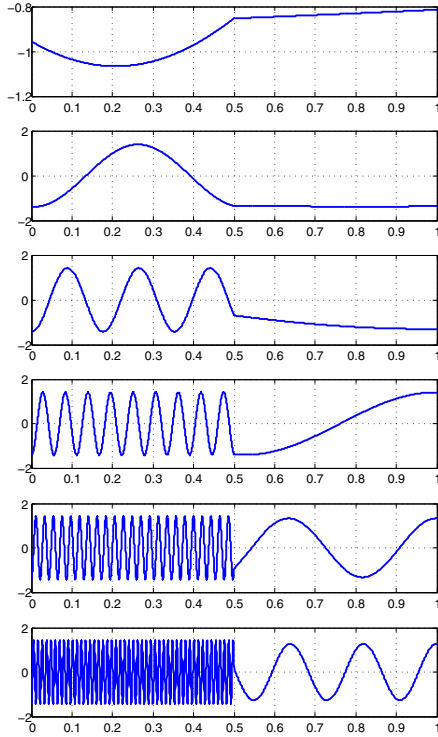


Fig. 1. Eigenfunctions $e_1, e_3, e_7, e_{20}, e_{50}, e_{100}$.

C. The Gevrey “step function” and its derivatives

It is well-known that the “bump function”

$$\phi_s(t) := \begin{cases} 0 & \text{if } t \notin (0, 1) \\ \exp\left(\frac{-1}{M^k(1-t)^k}\right) & \text{if } t \in (0, 1), \end{cases}$$

where $k = (s-1)^{-1}$ and $M > 0$, is Gevrey of order s ; and so is the Gevrey “step function”

$$\phi_s(t) := \begin{cases} 1 & \text{if } t \leq 0 \\ 0 & \text{if } t \geq 1 \\ 1 - \frac{\int_0^t \phi_s(\rho) d\rho}{\int_0^1 \phi_s(\rho) d\rho} & \text{if } t \in (0, 1), \end{cases}$$

used in (18) to design the flatness-based control. It is readily checked that $\phi_s(0) = 1$, $\phi_s^{(i)}(0) = 0$ for $i \geq 1$, and $\phi_s^{(i)}(1) = 0$ for $i \geq 0$.

A practical problem when implementing the control (19) is to evaluate sufficiently many derivatives of ϕ_s , i.e. of φ_s . This can be done easily as follows. We first note that

$$p^{k+1} \phi_s = k \dot{p} \phi_s, \quad (24)$$

where $p(t) := M^{\frac{1}{k}} t(1-t)$ is a polynomial of degree 2 (hence its derivatives of order > 2 are zero). We then apply the general Leibniz rule

$$(uv)^{(i)} = \sum_{j=0}^i \binom{i}{j} u^{(j)} v^{(i-j)}$$

to both sides of (24), yielding

$$P \varphi_s^{(i+1)} + \sum_{j=1}^i \binom{i}{j} P^{(j)} \varphi_s^{(i+1-j)} = k(\dot{p} \varphi_s^{(i)} + i \ddot{p} \varphi_s^{(i-1)}). \quad (25)$$

This is a recursion formula giving $\varphi_s^{(i+1)}$ in function of $\varphi_s^{(0)}, \dots, \varphi_s^{(i)}$ and the derivatives of $P := p^{k+1}$. The derivatives of P are obtained in the same manner, by applying the Leibniz rule to both sides of

$$p \dot{P} = (k+1) \dot{p} P,$$

yielding the recursion formula

$$p P^{(i+1)} = (k+1-i) \dot{p} P^{(i)} + \frac{i}{2} (2k+3-i) \ddot{p} P^{(i-1)}. \quad (26)$$

To avoid computing ratios of very large numbers, it is in practice better to use recursion formulas for $\tilde{P}^{(i)} := \frac{P^{(i)}}{i!}$ and $\tilde{\varphi}_s^{(i)} := \frac{\varphi_s^{(i)}}{(2i)!}$. From (26) and (25), we find

$$p \tilde{P}^{(i+1)} = \frac{1}{i+1} \left[(k+1-i) \dot{p} \tilde{P}^{(i)} + \frac{2k+3-i}{2} \ddot{p} \tilde{P}^{(i-1)} \right]$$

$$\tilde{P} \tilde{\varphi}_s^{(i+1)} = \frac{k}{(2i+2)(2i+1)} \left[\dot{p} \tilde{\varphi}_s^{(i)} + \frac{\ddot{p} \tilde{\varphi}_s^{(i-1)}}{2(2i-1)} \right]$$

$$- \sum_{j=1}^i d_{i+1,j} \tilde{P}^{(j)} \tilde{\varphi}_s^{(i+1-j)}$$

$$d_{i+1,0} = 1$$

$$d_{i+1,j} = \frac{i-j+1}{(2i-2j+4)(2i-2j+3)} d_{i+1,j-1}, \quad j = 1, \dots, i.$$

Using this procedure, about 140 derivatives can be efficiently determined with Matlab double-precision arithmetics.

IV. NUMERICAL EXPERIMENTS

We now show some numerical results, using as parameters

X	a_0	ρ_0	a_1	ρ_1	α_0	β_0	α_1	α_1
$\frac{1}{2}$	$\frac{10}{19}$	$\frac{15}{8}$	10	$\frac{1}{8}$	$\cos \frac{\pi}{3}$	$-\sin \frac{\pi}{3}$	$\cos \frac{\pi}{4}$	$\sin \frac{\pi}{4}$

The initial condition $\theta_0 \in L^2(0, 1)$ is the step function $\theta_0(x) = -\frac{1}{2}$ on $(0, \frac{1}{2})$ and $\theta_0(x) = \frac{1}{2}$ on $(\frac{1}{2}, 1)$; θ_0 not being continuous, its coefficients c_n decay slowly. The final time is $T = 0.35$; several values of the intermediate time τ are used, namely $\tau = 0.01, 0.05, 0.1, 0.15$, to see its influence. Finally $s = 1.65$ and $M = 2$ for the base case (recall s and M are the coefficients in the Gevrey “step function”); these values are later changed one at a time to see their influences. The series for u and y in (18) and (19) were truncated at a “large enough” order for a good accuracy, namely $\bar{i} = 130$ and $\bar{n} = 60$; a fairly large \bar{i} is needed here because $(T - \tau)\frac{a_0}{\rho_0}$ is rather small. The error on the trajectory due to these truncations is expected to behave well, provided that the uniform estimates proved in [10] in a much simpler situation are generalizable. Also note that the control effort, as well as the truncation index \bar{i} needed to ensure a good accuracy of u , grows rapidly as T decreases.

Fig. 2 shows the evolution of the control $u(t)$ and Fig. 3 the evolution of the control energy $(\int_0^t u^2(s)ds)^{\frac{1}{2}}$; it appears that the control effort increases with τ (for a given T), with a more oscillatory behavior. Fig. 4 shows the resulting temperature θ (for $\tau = 0.05$ only); the discontinuity of θ_x at $x = X$ is clearly visible. Fig. 5 and Fig. 6 show the evolution of the control and of its energy when $M = 1$, and so do Fig. 7 and Fig. 8 when $s = 2.5$; it appears that the control effort decreases as M increases, but at the expense of a more oscillatory behavior (and a higher \bar{i} for a good accuracy of u). Finally, Fig. 9 and Fig. 10 show the evolution of the control and of the control energy when $s = 1.45$, and so do Fig. 11 and Fig. 12 when $s = 1.5$; it appears that the control effort decreases as s increases, but at the expense of a more oscillatory behavior (and a higher \bar{i} for a good accuracy of u). Of course these few qualitative remarks should be taken with caution, as they are yet to be backed by theory.

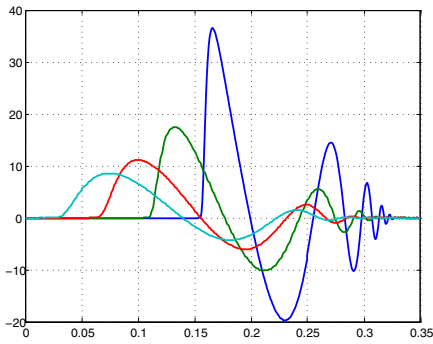


Fig. 2. Base case: evolution of the control $u(t)$.

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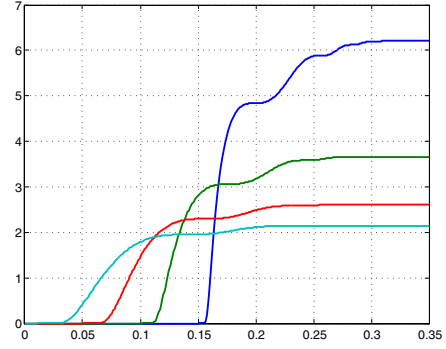


Fig. 3. Base case: evolution of the control energy $(\int_0^t u^2(s)ds)^{\frac{1}{2}}$.

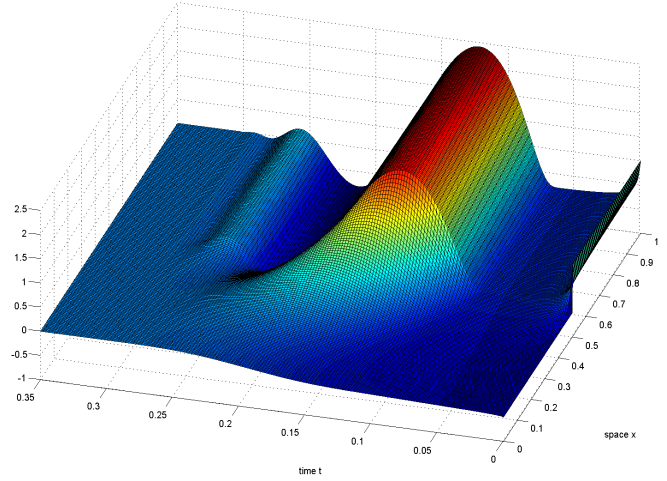


Fig. 4. Evolution of the temperature $\theta(t, x)$.

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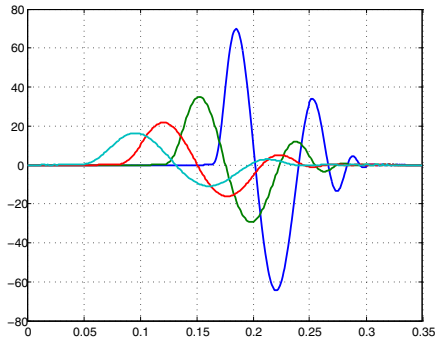


Fig. 5. $M = 1$: evolution of the control $u(t)$.

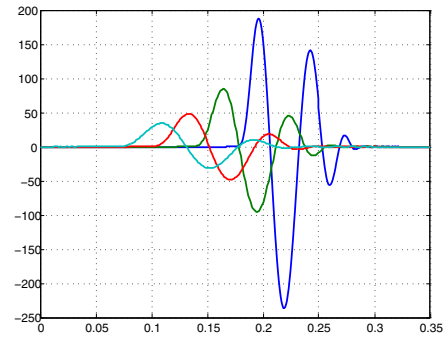


Fig. 9. $s = 1.45$: evolution of the control $u(t)$.

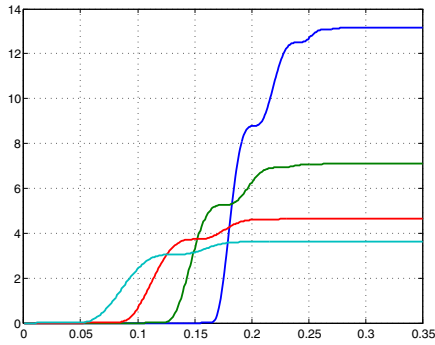


Fig. 6. $M = 1$: evolution of the control energy $(\int_0^t u^2(s)ds)^{\frac{1}{2}}$.

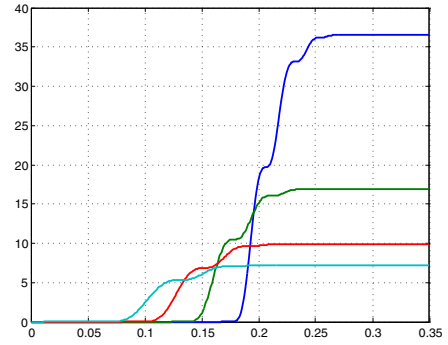


Fig. 10. $s = 1.45$: evolution of the control energy $(\int_0^t u^2(s)ds)^{\frac{1}{2}}$.

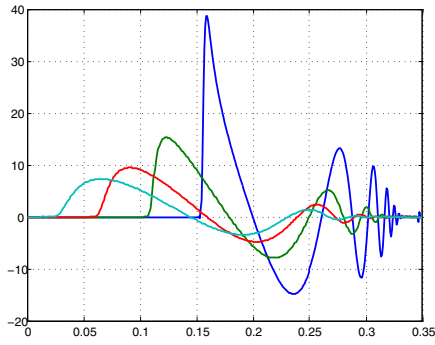


Fig. 7. $M = 2.5$: evolution of the control $u(t)$.

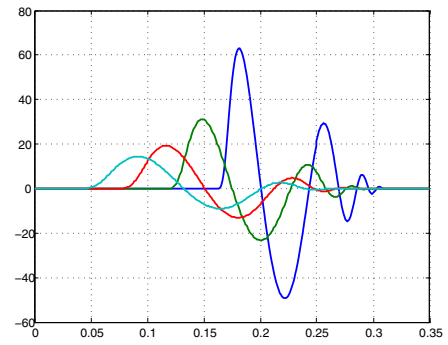


Fig. 11. $s = 1.55$: evolution of the control $u(t)$.

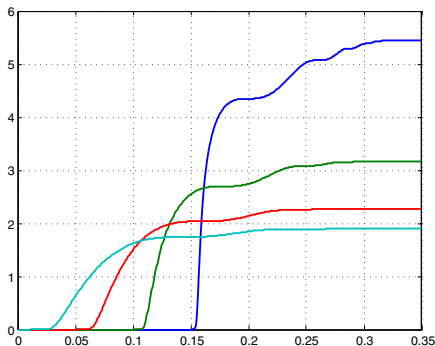


Fig. 8. $M = 2.5$: evolution of the control energy $(\int_0^t u^2(s)ds)^{\frac{1}{2}}$.

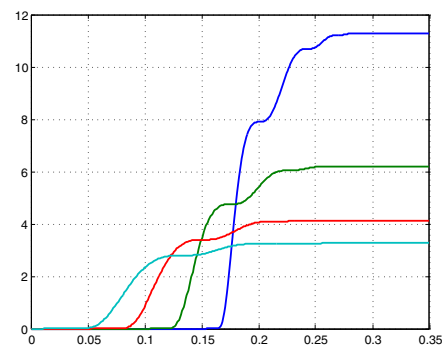


Fig. 12. $s = 1.55$: evolution of the control energy $(\int_0^t u^2(s)ds)^{\frac{1}{2}}$.